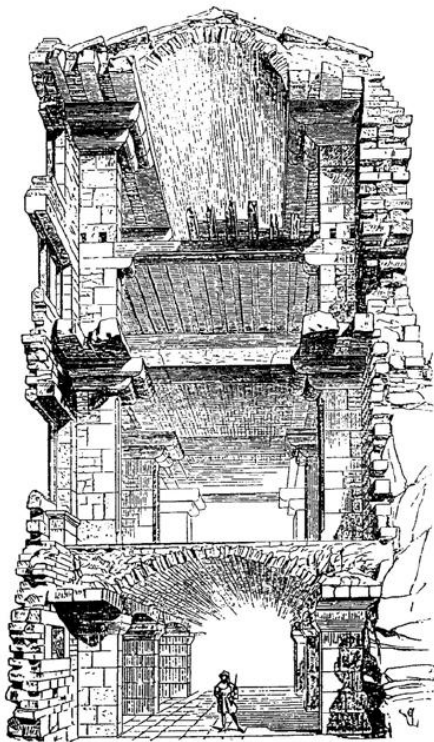


Design of Self-supporting Surfaces

Etienne Vouga	Columbia University
Mathias Höbinger	Evolute / TU Wien
Johannes Wallner	TU Graz / TU Wien
Helmut Pottmann	KAUST



[Viollet-le-Duc 1858]



[Gaudí. Photo by Flickr user "SBA73"]



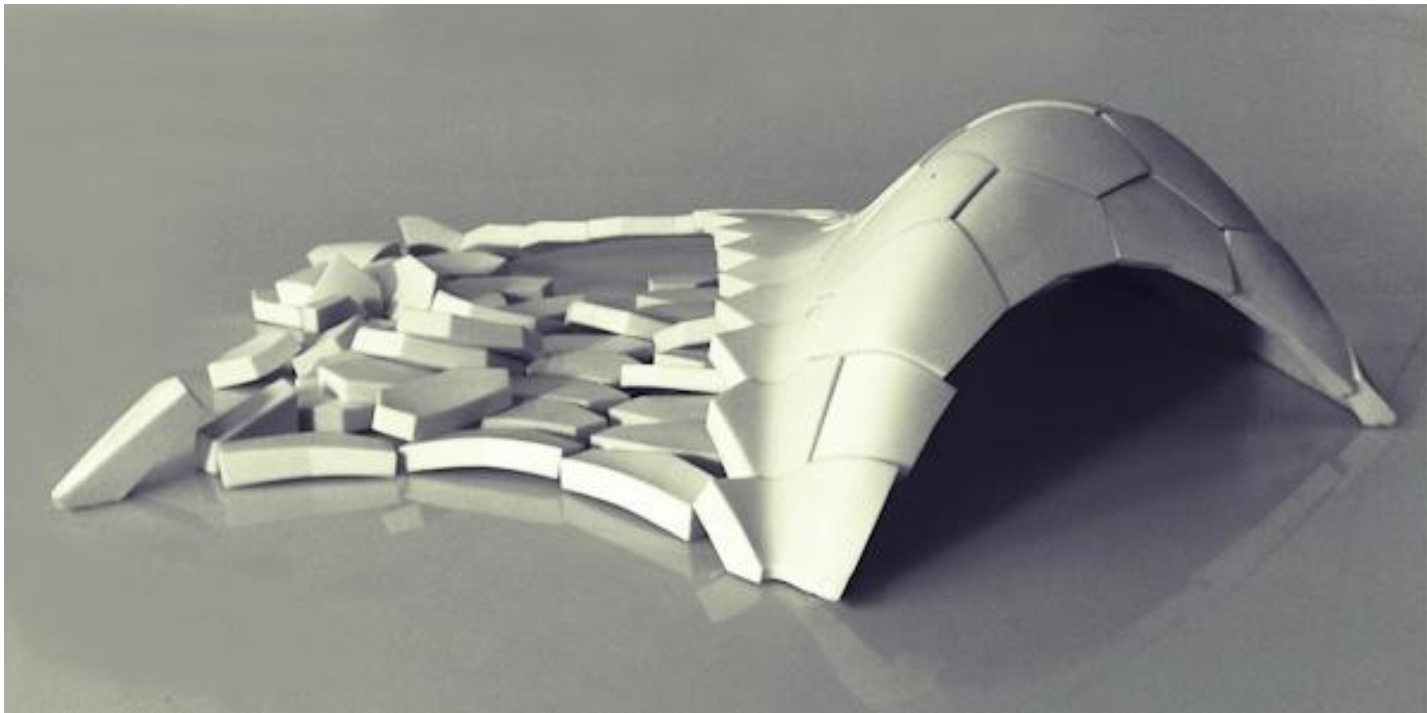
[Ramage et al 2008]



[Sobek 2008]

Why Masonry?

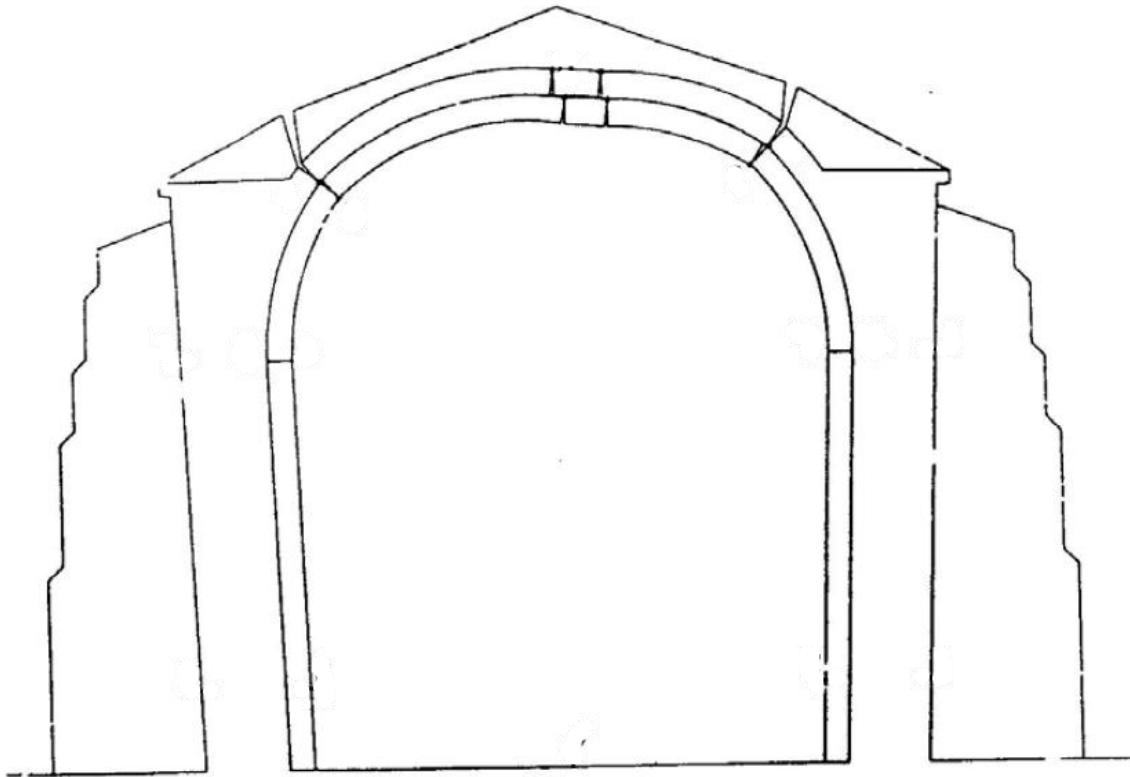
Material failure is unimportant: masonry structures fail due to *bad geometry*



[Philippe Block]

Why Masonry?

“Small elastic displacements” incorrect deformation model



[Huerta and López 1997]



[Photo by Flickr user "arcticpenguin"]

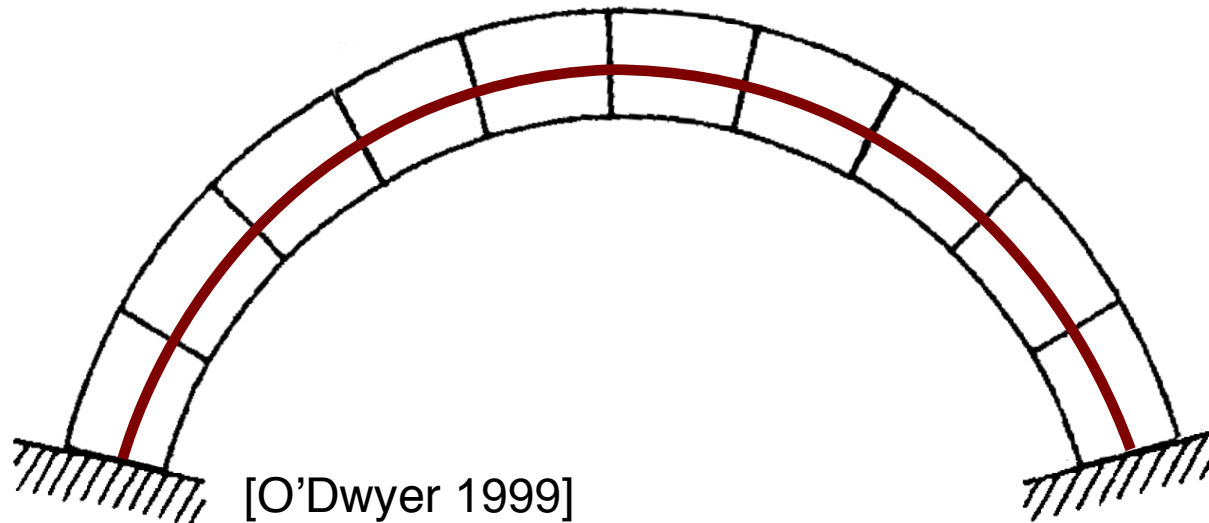
A photograph of a Gothic cathedral ceiling, showing a complex ribbed vault structure. The ribs are made of stone and are supported by a network of smaller ribs, creating a series of pointed arches. The ceiling is made of stone blocks, and the overall structure is highly detailed and ornate. The lighting is warm, highlighting the texture of the stone and the intricate geometry of the vaulting.

Can we interactively design these structures?

Can we understand their geometry?

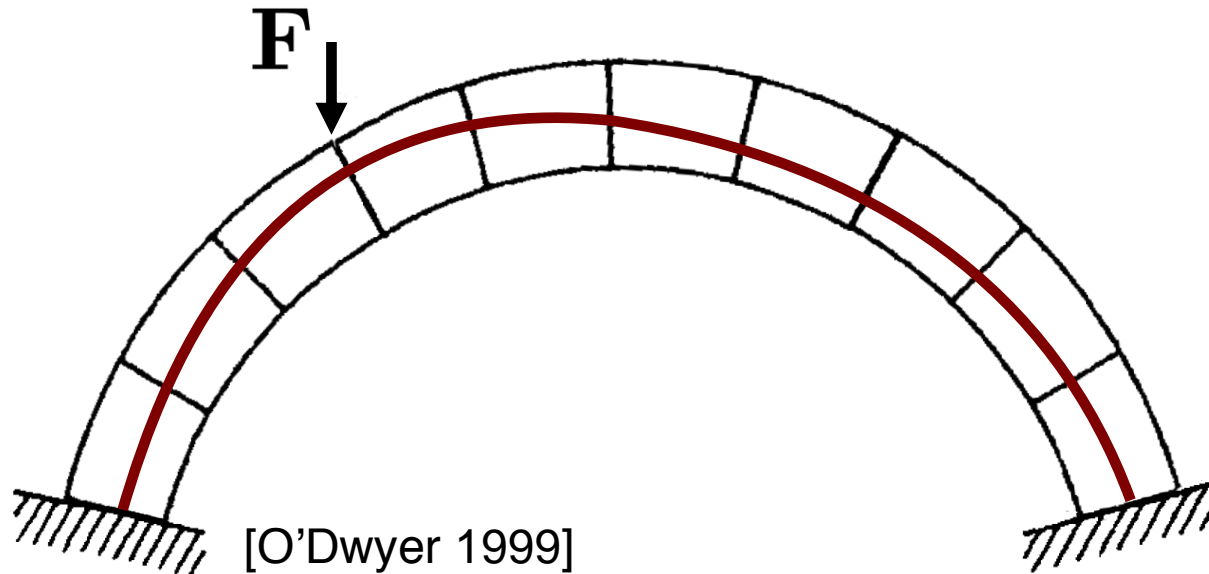
Safe Theorem [Heyman]

If embedded membrane
is stable, so is structure



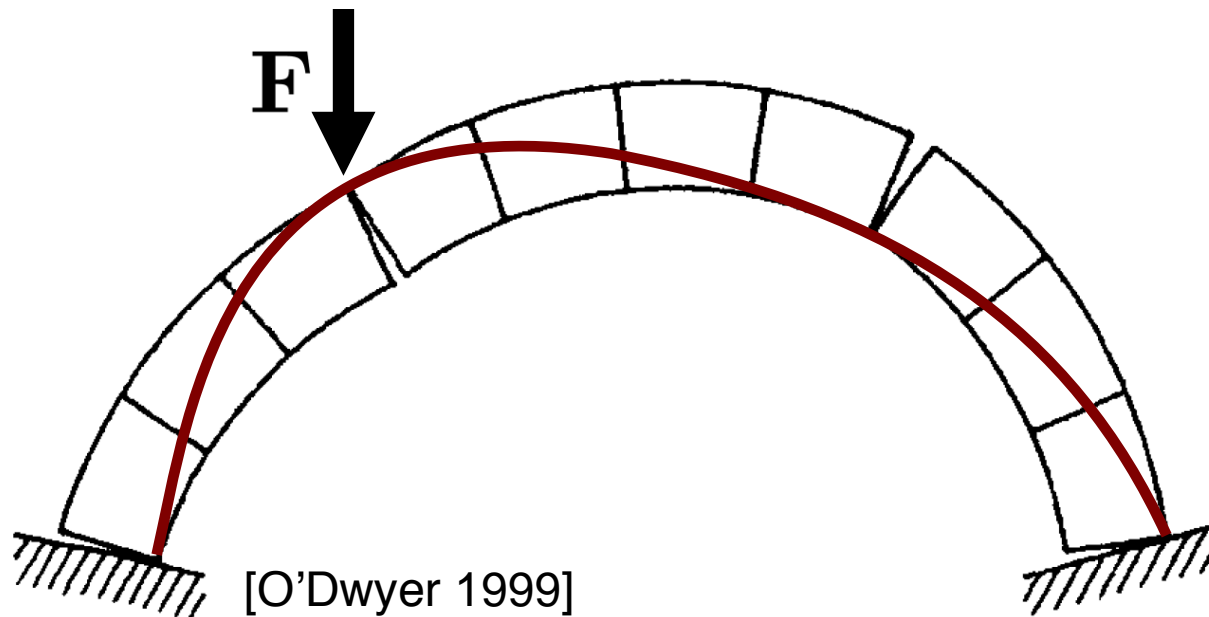
Safe Theorem [Heyman]

If embedded membrane is stable, so is structure



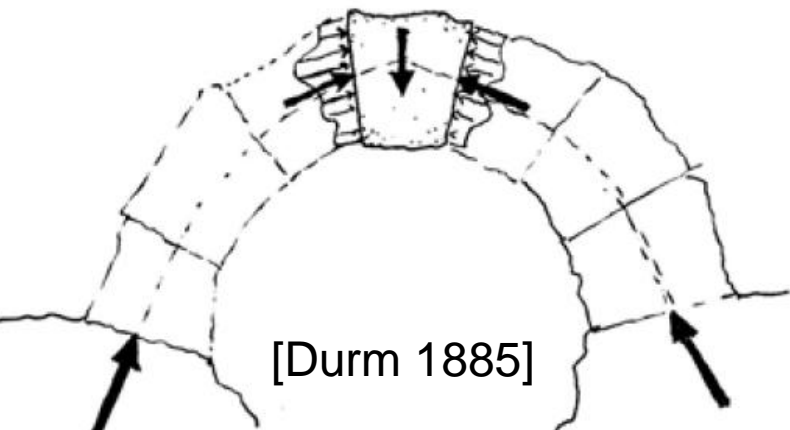
Safe Theorem [Heyman]

If embedded membrane is stable, so is structure

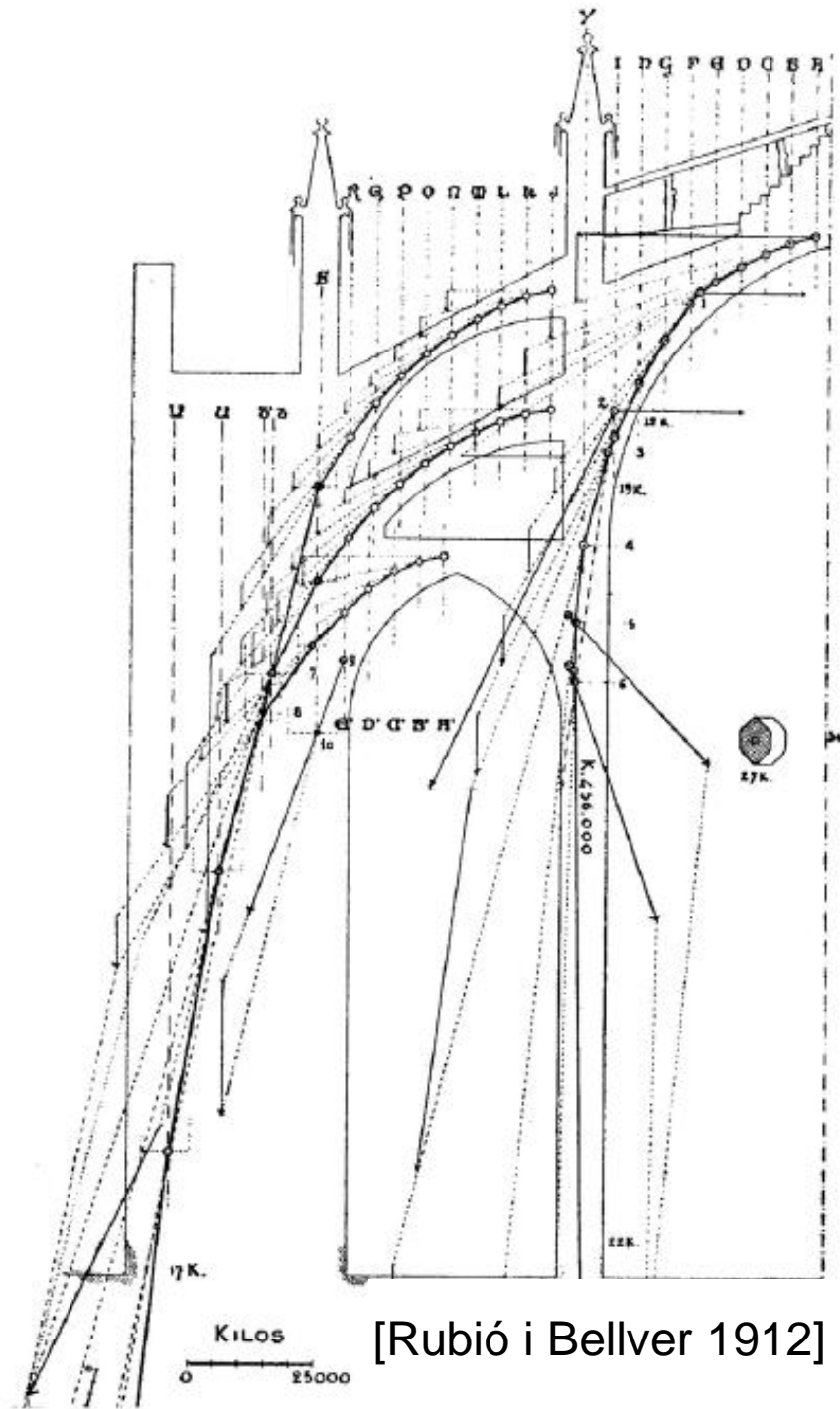


Safe Theorem [Heyman]

If embedded membrane is stable, so is structure



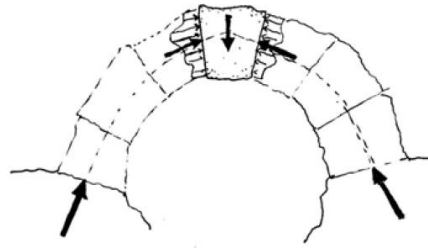
[Durm 1885]



[Rubió i Bellver 1912]

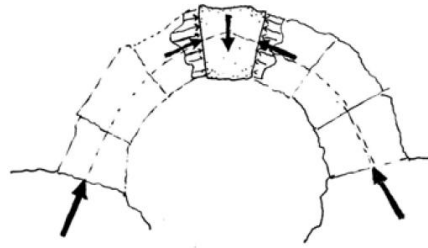
Modeling Assumptions

Safe Theorem



Modeling Assumptions

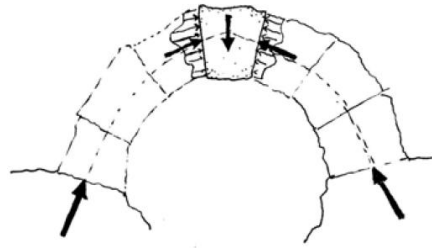
Safe Theorem



Infinite compressive, no tensile strength

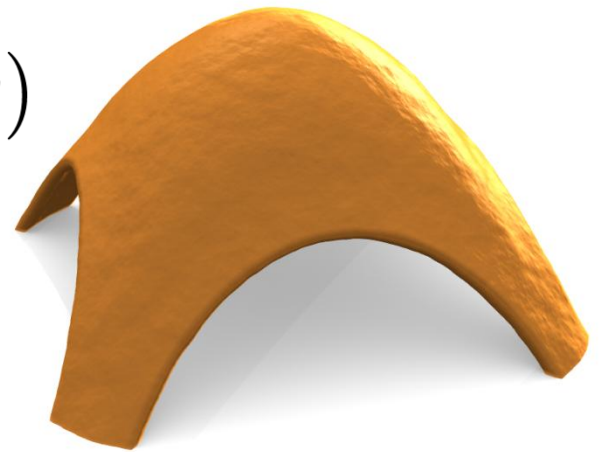
Modeling Assumptions

Safe Theorem



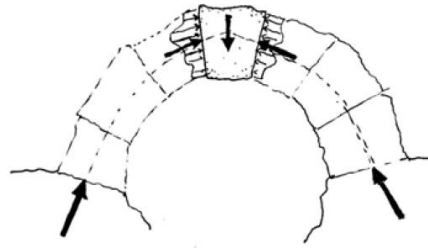
Infinite compressive, no tensile strength

Surface is height field $z(x, y)$



Modeling Assumptions

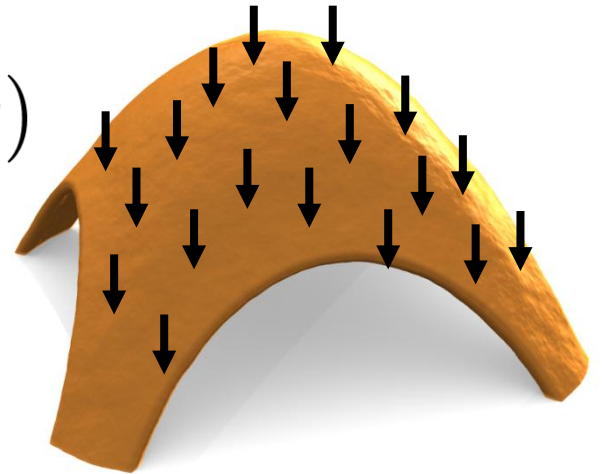
Safe Theorem



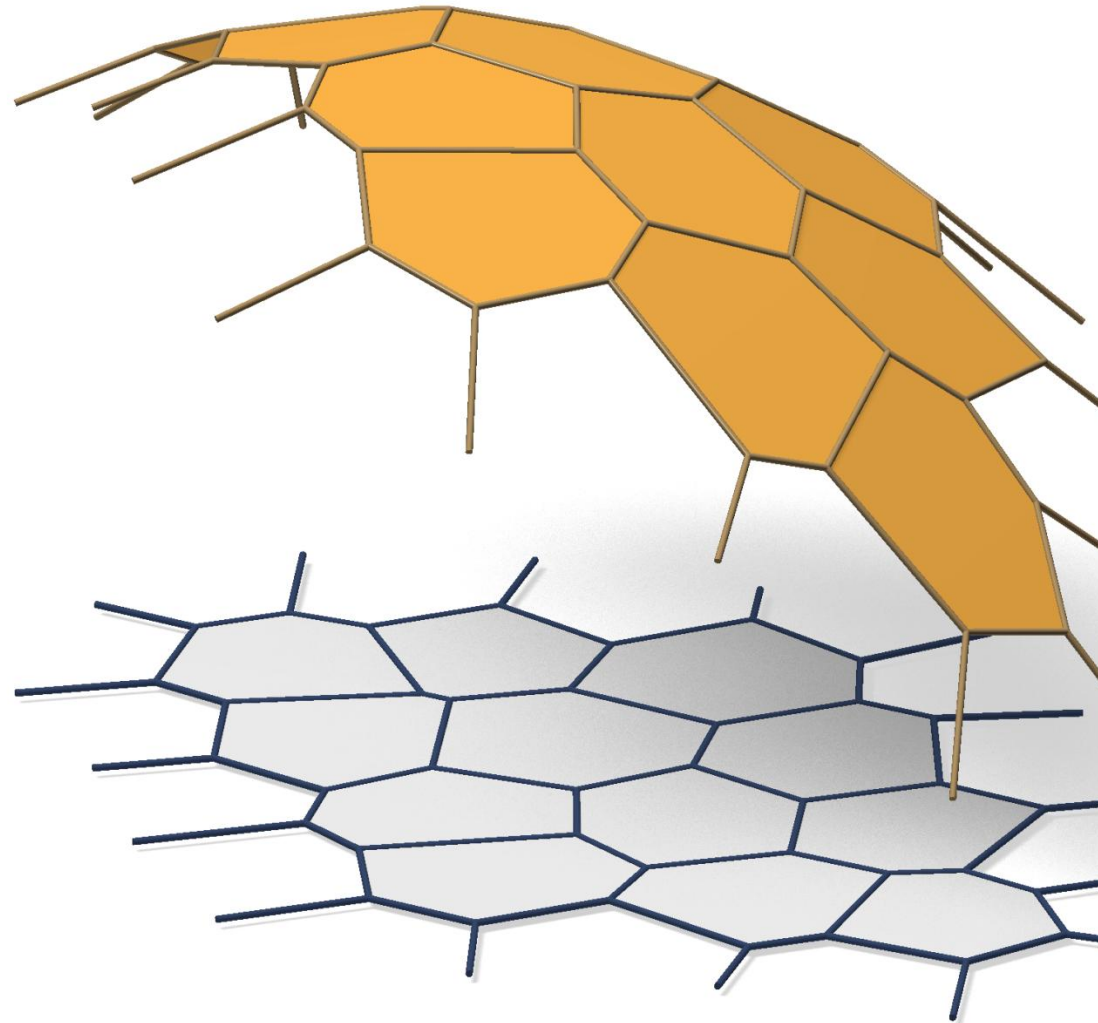
Infinite compressive, no tensile strength

Surface is height field $z(x, y)$

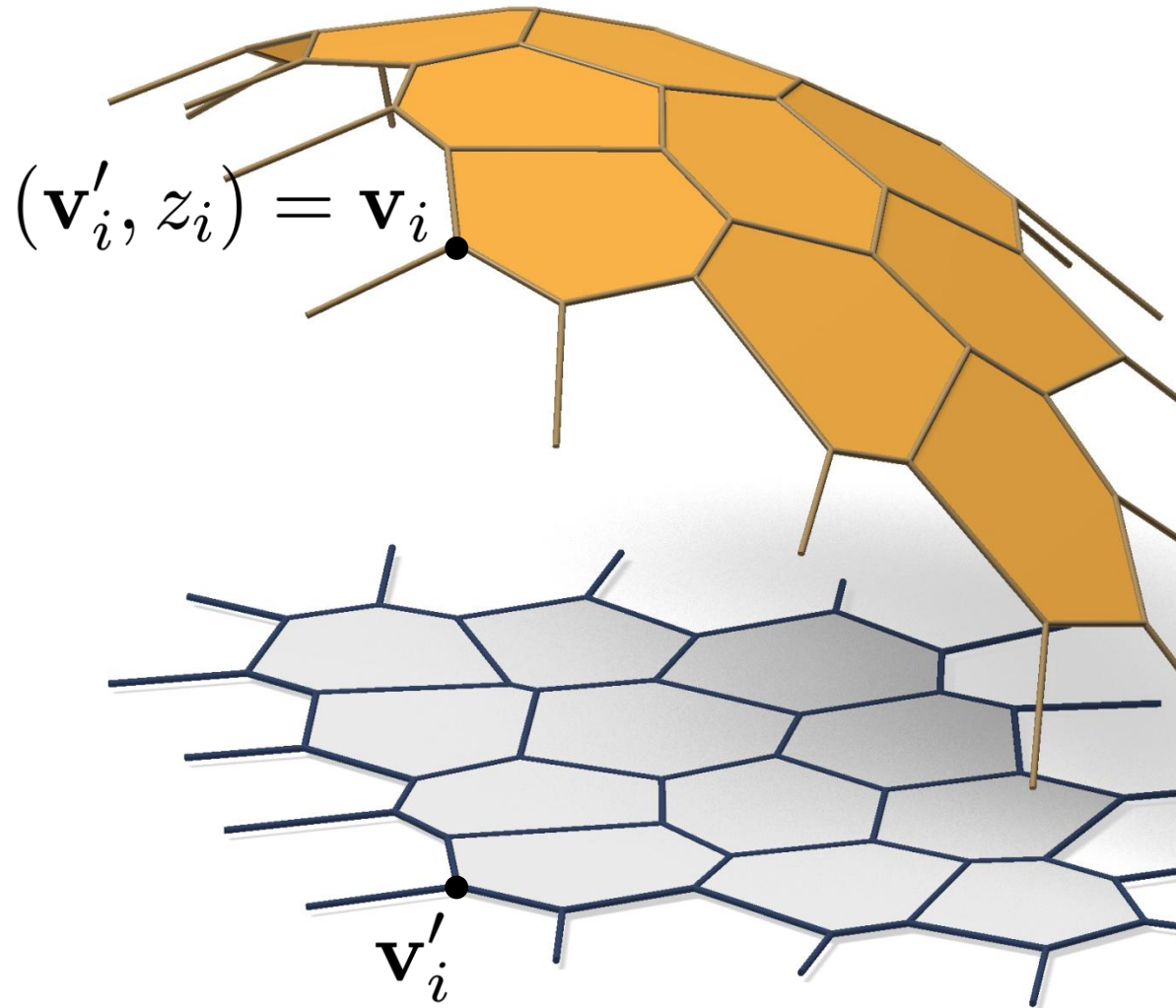
Loads are vertical



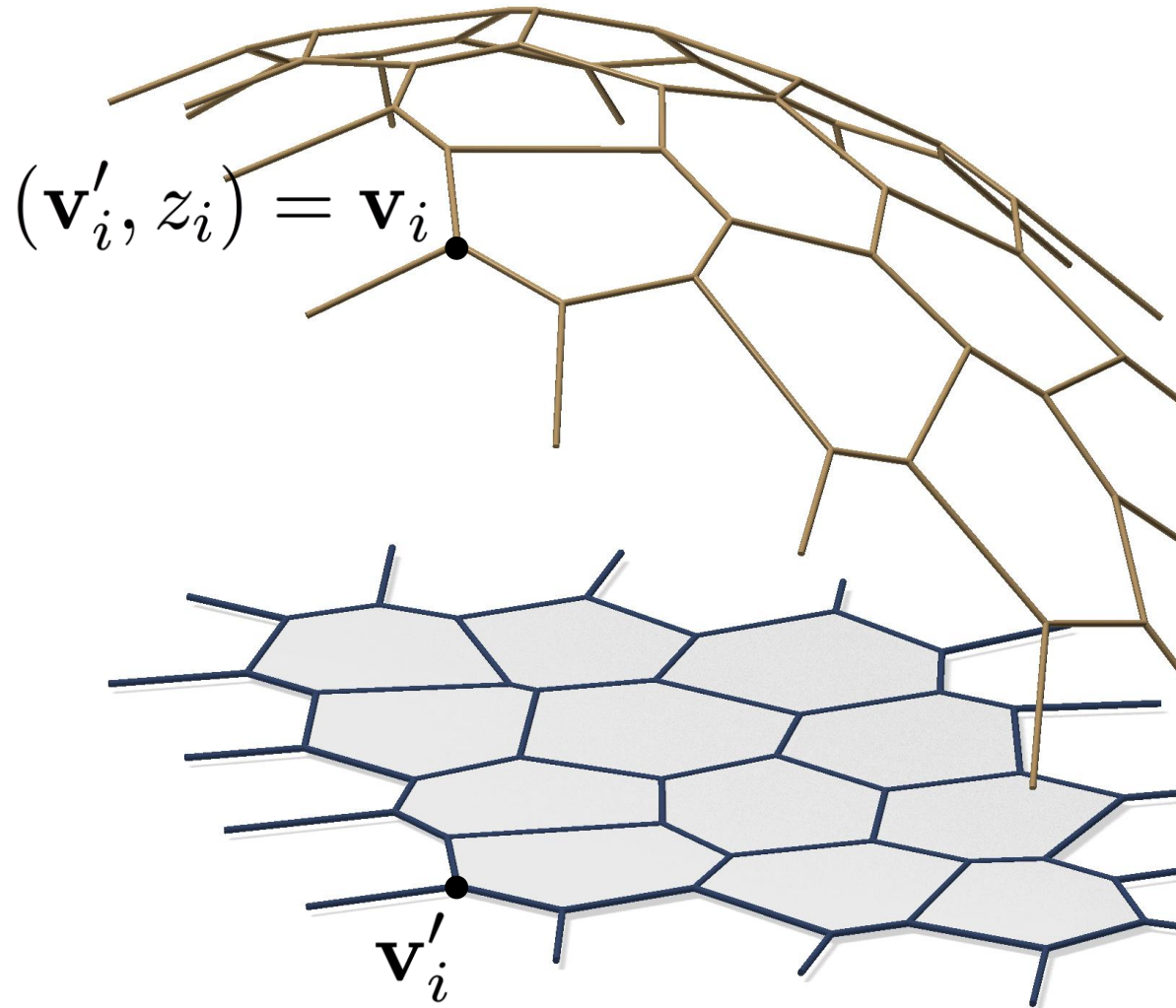
Discrete Thrust Network [Block 2009]



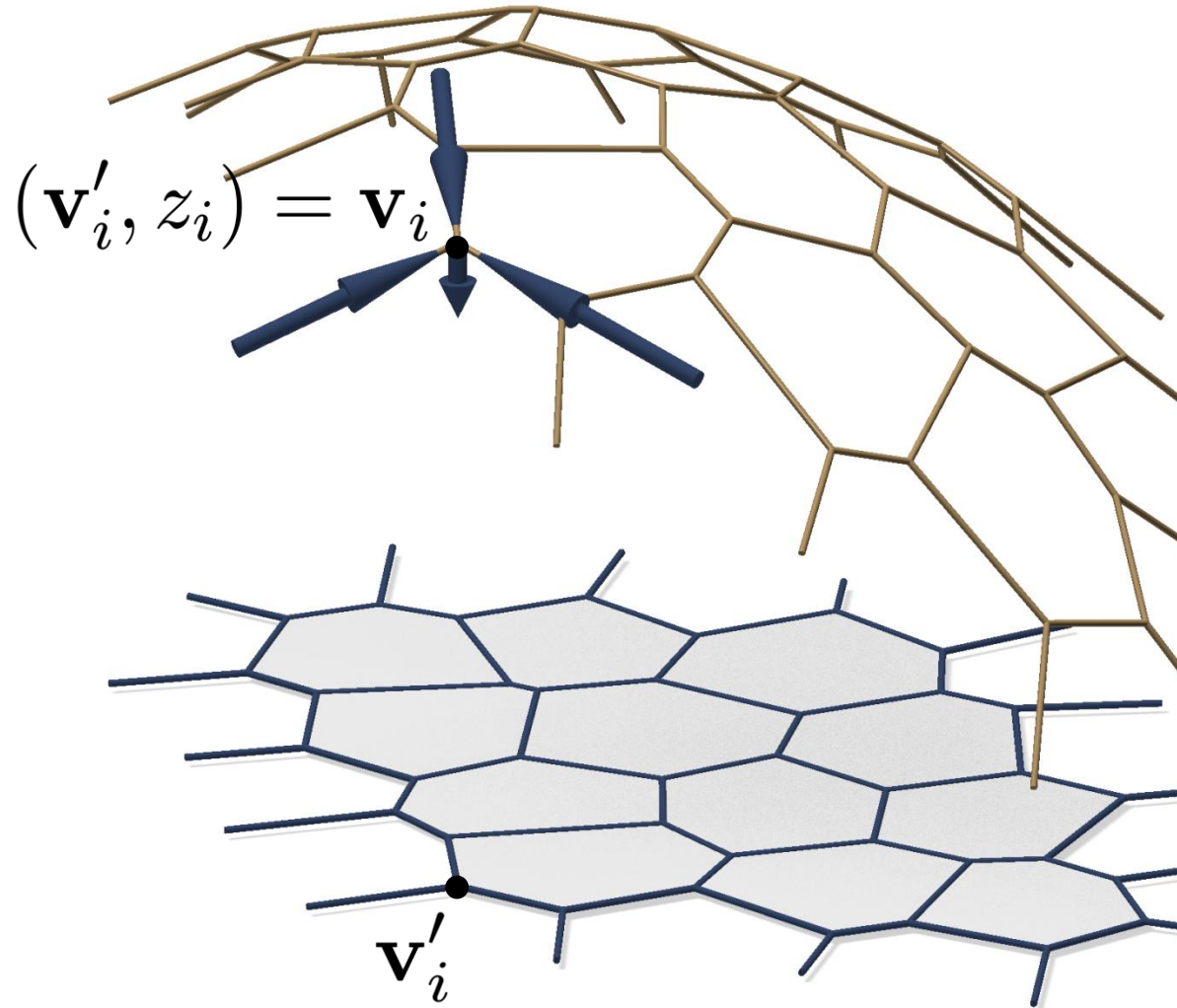
Discrete Thrust Network [Block 2009]



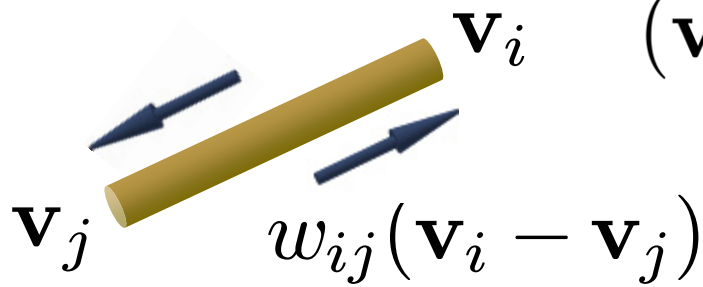
Discrete Thrust Network [Block 2009]



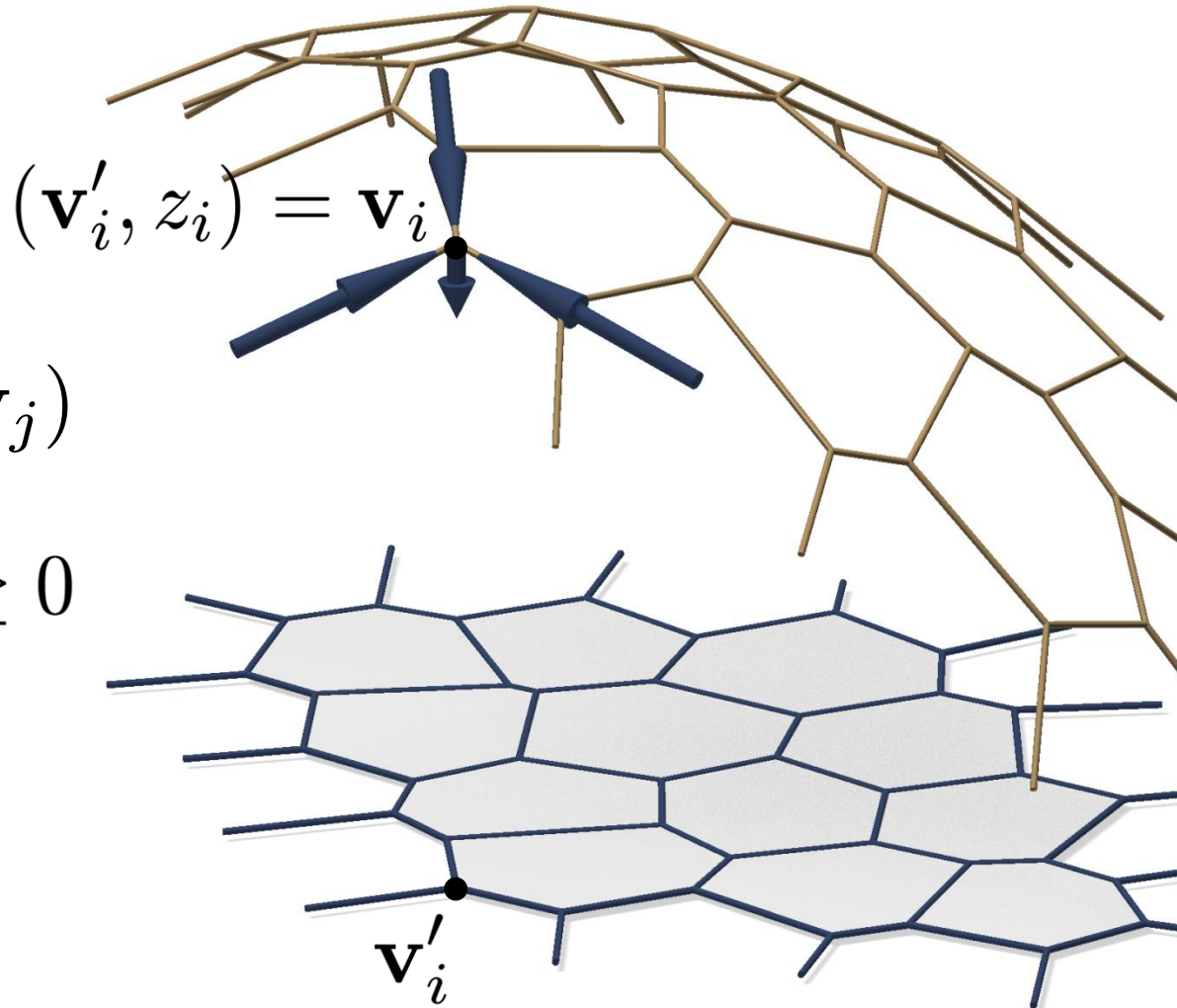
Discrete Thrust Network [Block 2009]



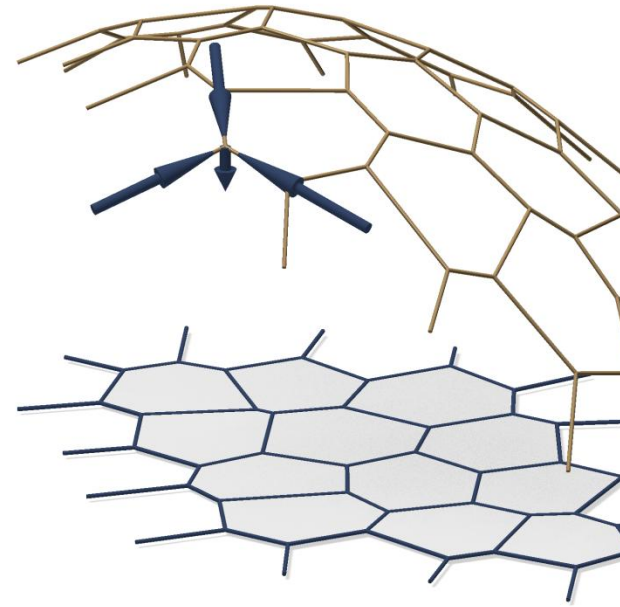
Discrete Thrust Network [Block 2009]



compressive: $w_{ij} \geq 0$



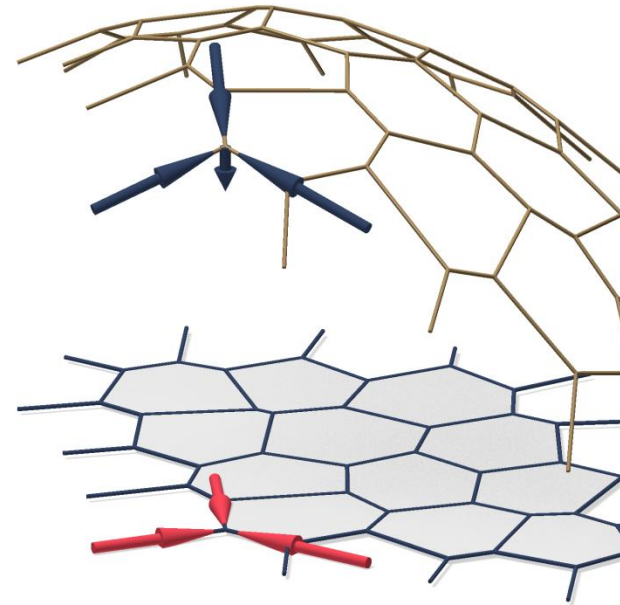
Equilibrium Equations



Equilibrium Equations

Horizontal equilibrium:

$$\sum_{j \sim i} w_{ij} (\mathbf{v}'_i - \mathbf{v}'_j) = 0$$



Equilibrium Equations

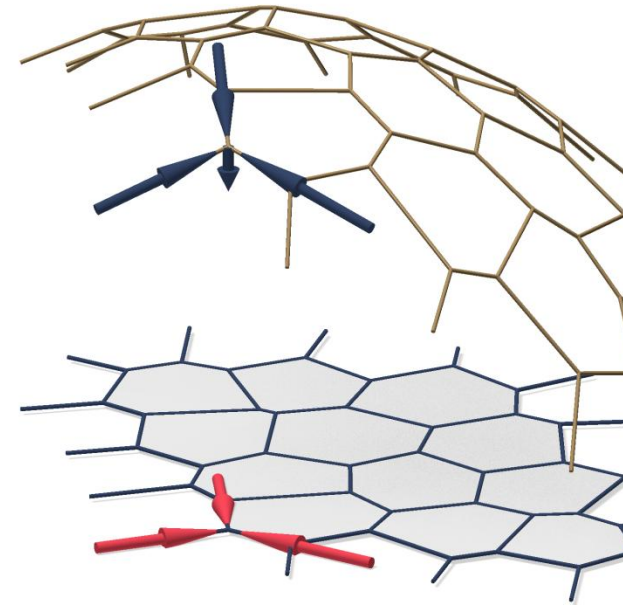
Horizontal equilibrium:

$$\sum_{j \sim i} w_{ij} (\mathbf{v}'_i - \mathbf{v}'_j) = 0$$

Vertical equilibrium:

$$\sum_{j \sim i} w_{ij} (z_i - z_j) = -A_i F_i$$

gravity of lumped mass
↓



Historical Perspective



Photo: Flickr user "tillnm"



Antoni Gaudí
1852-1926

Historical Perspective



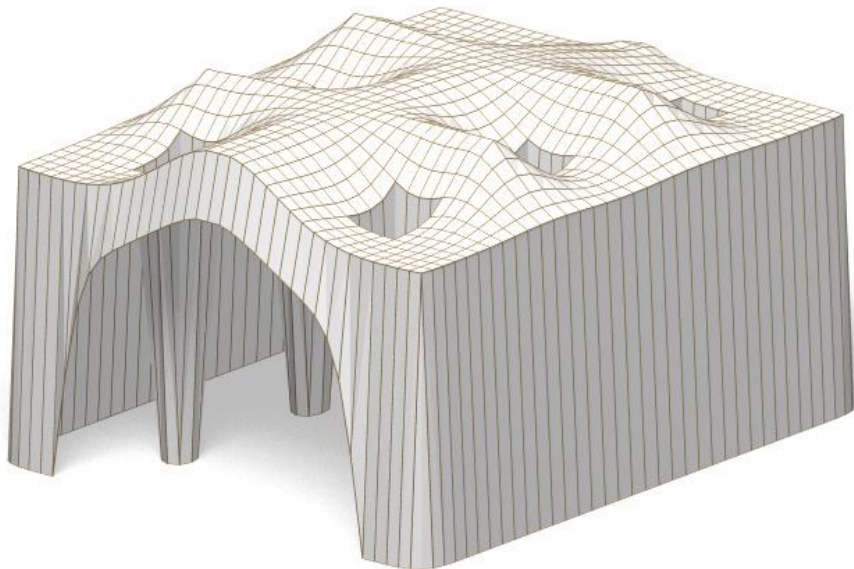
Photo: Flickr user "tillnm"



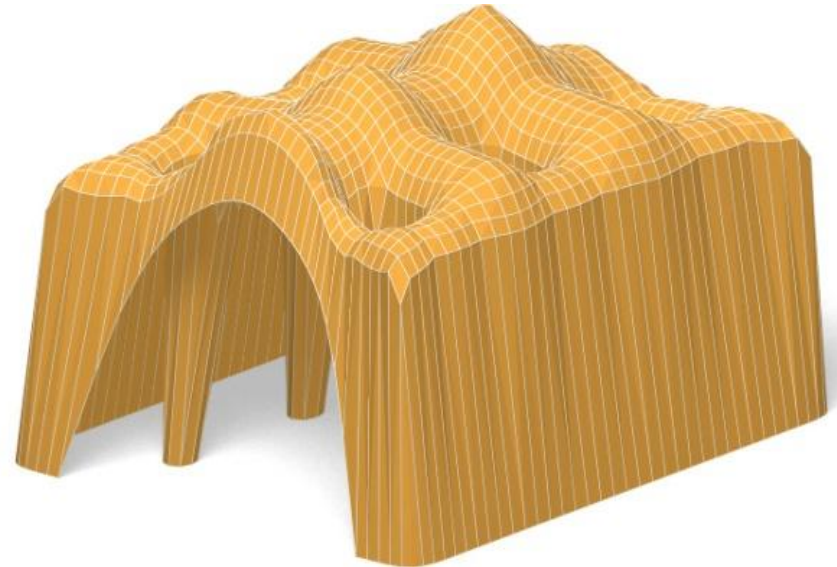
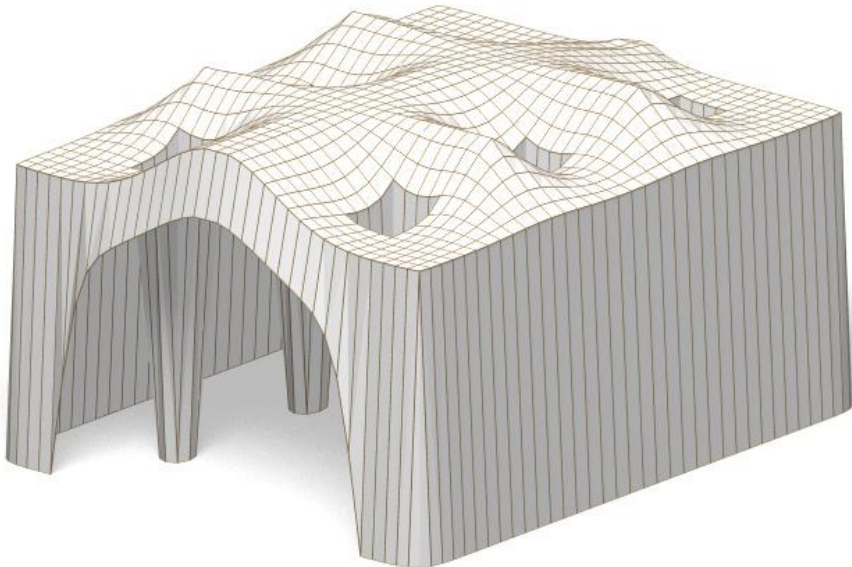
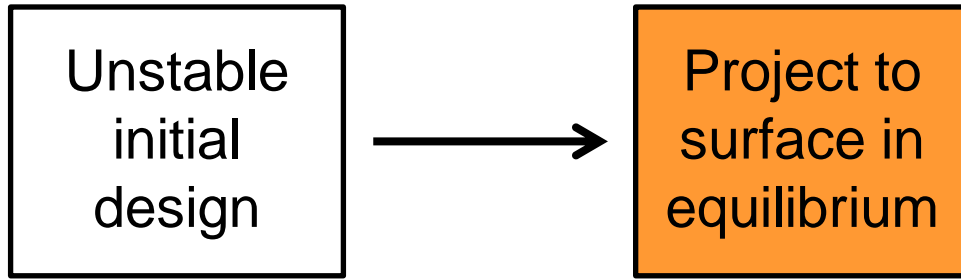
Colonia Güell, Gaudí

Design Paradigm

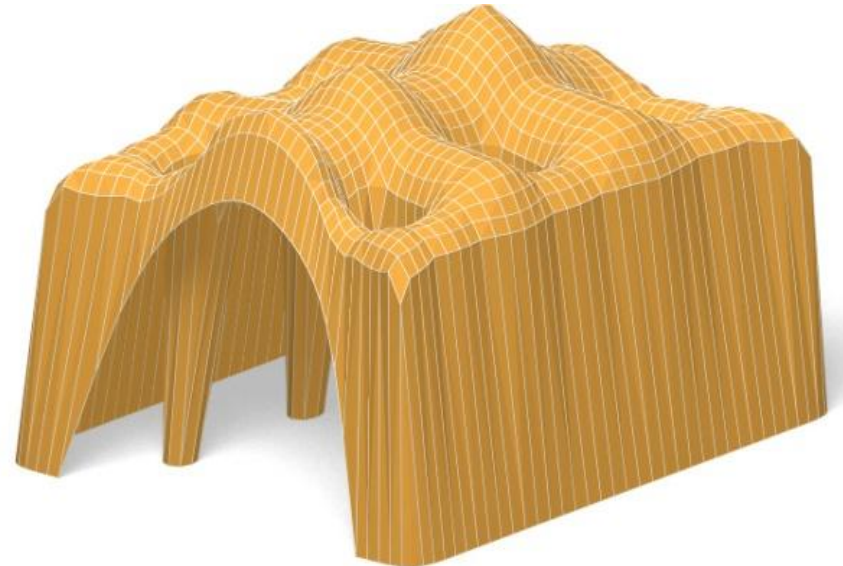
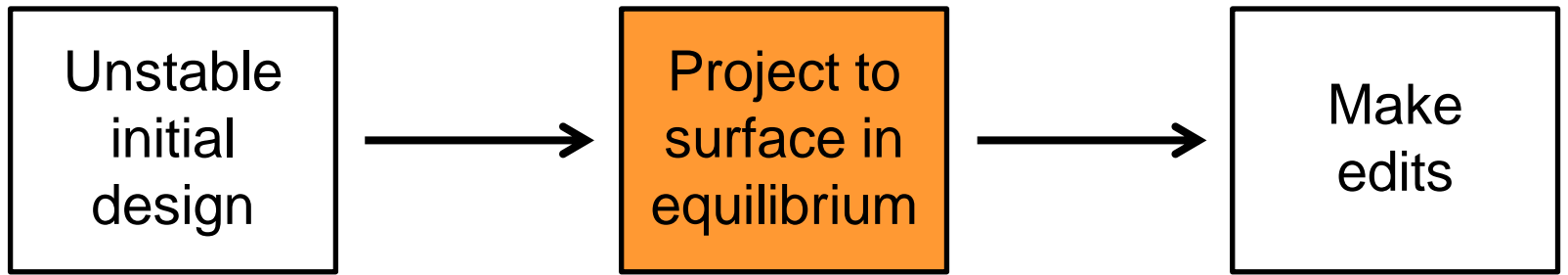
Unstable
initial
design



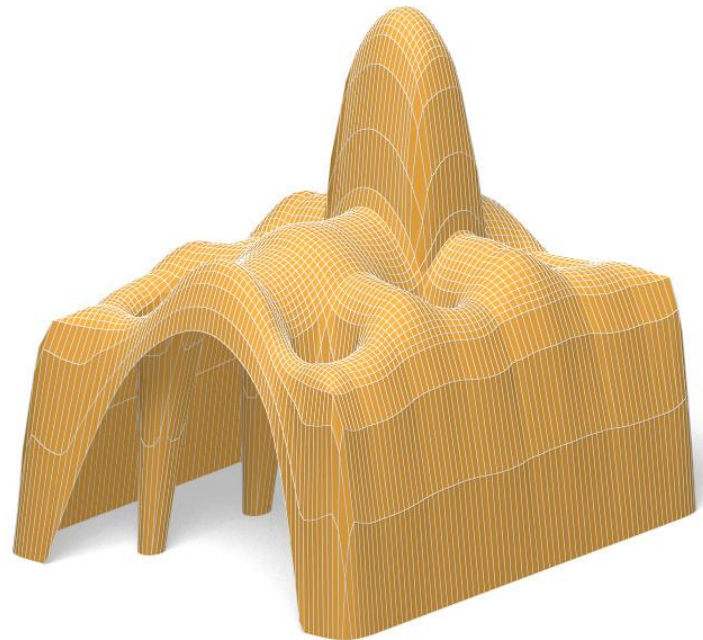
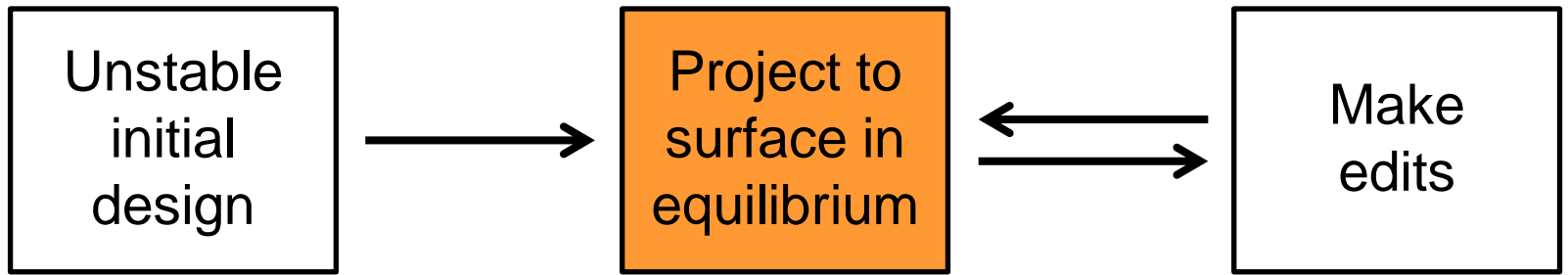
Design Paradigm



Design Paradigm



Design Paradigm



recall:

$$\sum w_{ij}(z_i - z_j) = -A_i F_i$$

$$\sum w_{ij}(\mathbf{v}'_i - \mathbf{v}'_j) = 0$$

$$w_{ij} \geq 0$$

Surface Projection

Until convergence:

nonlinear in positions



1. Calculate vertical forces $A_i F_i$

2. With positions fixed, find best weights

$$\min_{w_{ij}} \|\mathbf{F}_{\text{net}}\|^2 \quad \text{s.t.} \quad w_{ij} \geq 0$$

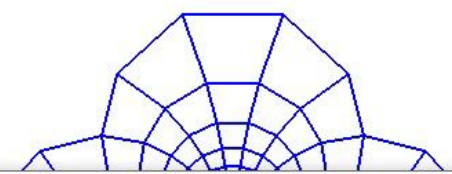
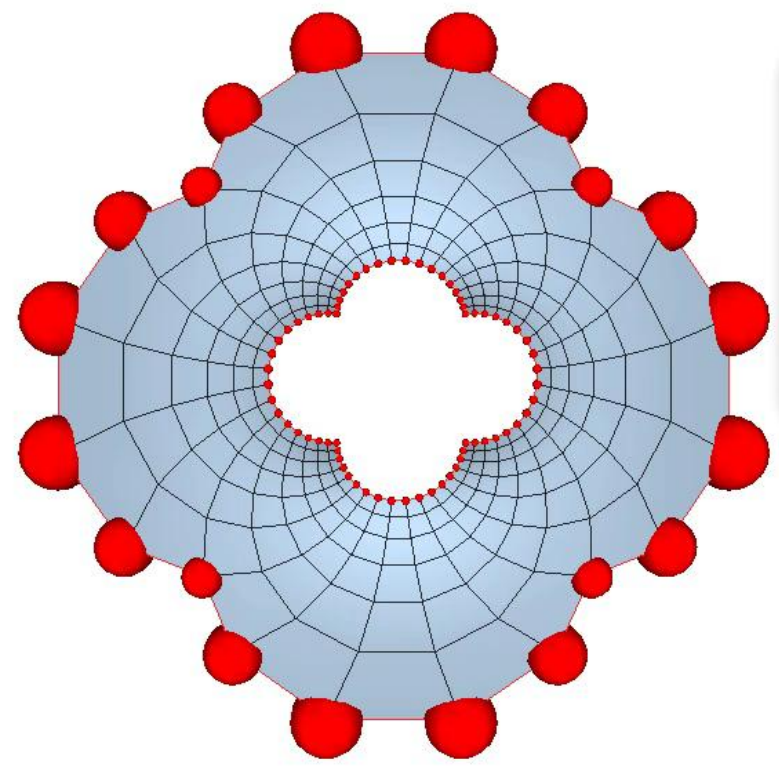
3. With weights fixed, perturb positions

$$\min_{\mathbf{u}} \|\mathbf{F}_{\text{net}}\|^2 + \alpha \|\mathbf{u}\|^2 + \beta \|\mathbf{u} \cdot \hat{\mathbf{n}}\|^2$$

penalize total and normal motion

Constrain Max Stress
1e9 N/m²

Delete black Compute Heights Dilate 0 Edge-flip



recordMyDesktop

Video Quality 100

Sound Quality 100

Advanced

Left click and drag, on the preview image, to select an area for recording.
Right click on it, to reset the area.

Select Window Record Save As Quit

Edit Mode

- Camera
- Handle (freeform)
- Handle (height)
- Handle (top)
- Delete Faces
- Pin
- Anchor
- Edge Collapse

Influence

Density: kg/m³ Thickness: m

Verts: Edge: Max rel equi. error:

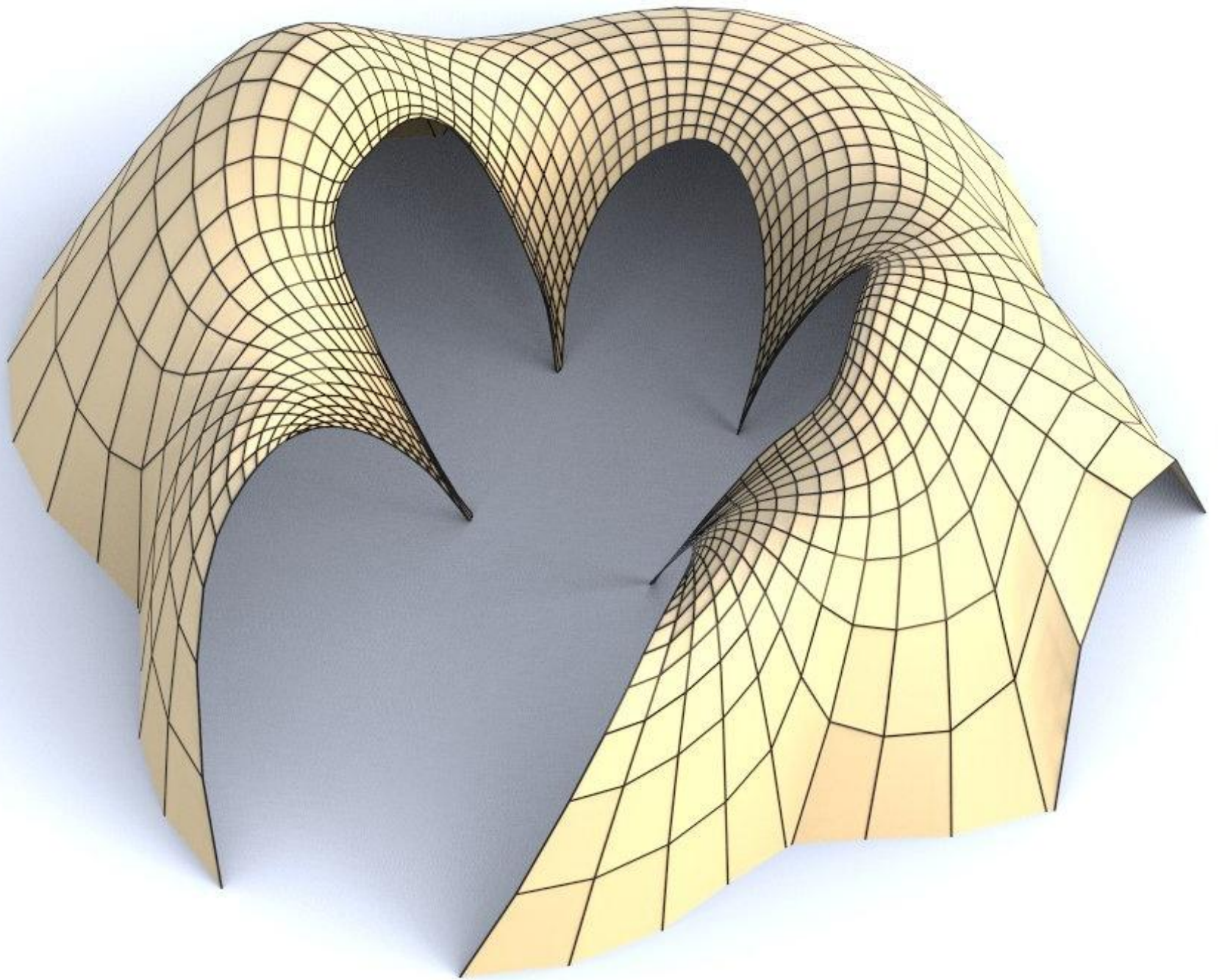
Render Options

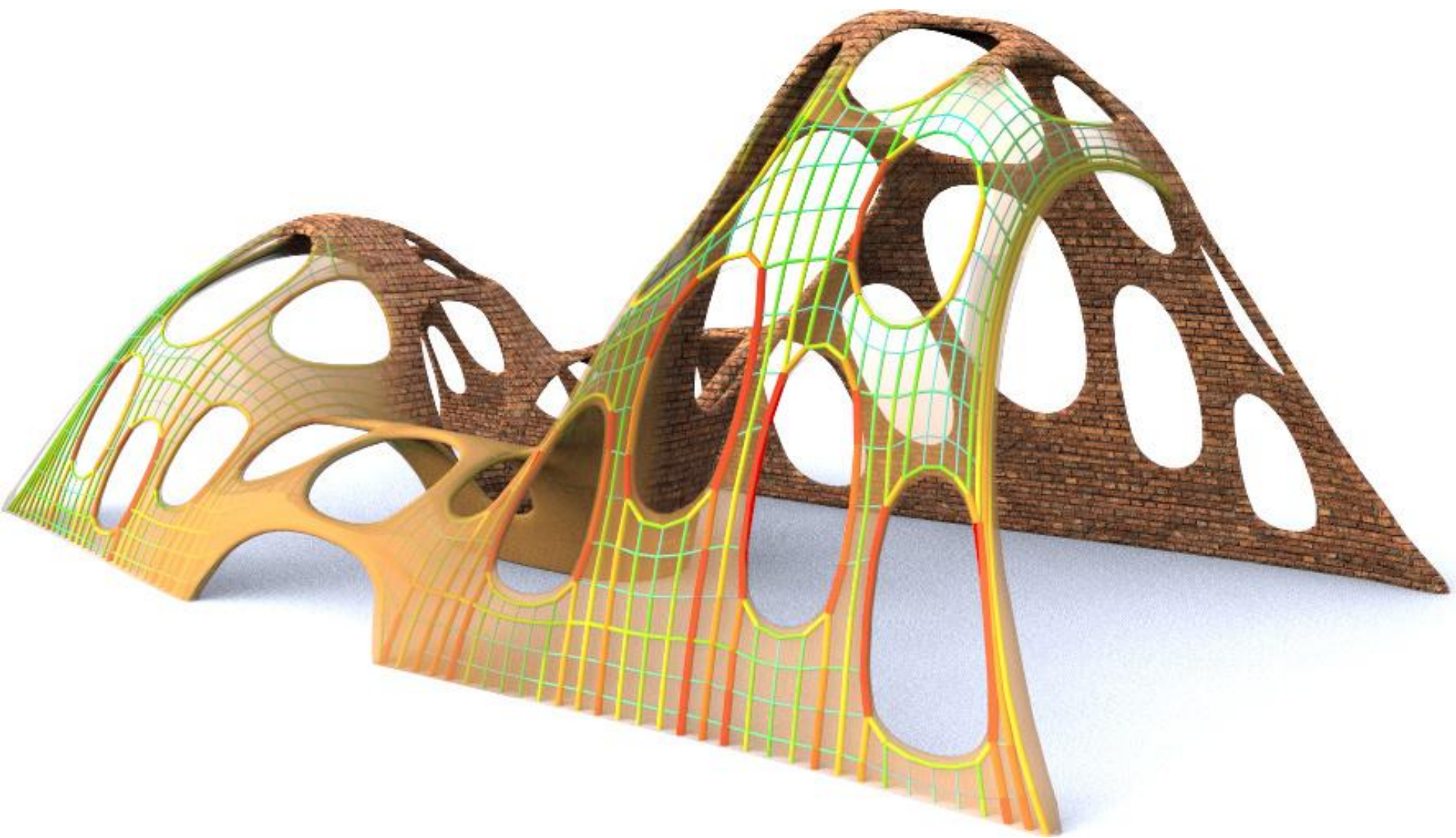
- Show reference surface
- Show thrust network
- Show thrust network surface
- Show stress surface
- Show conjugate vectors

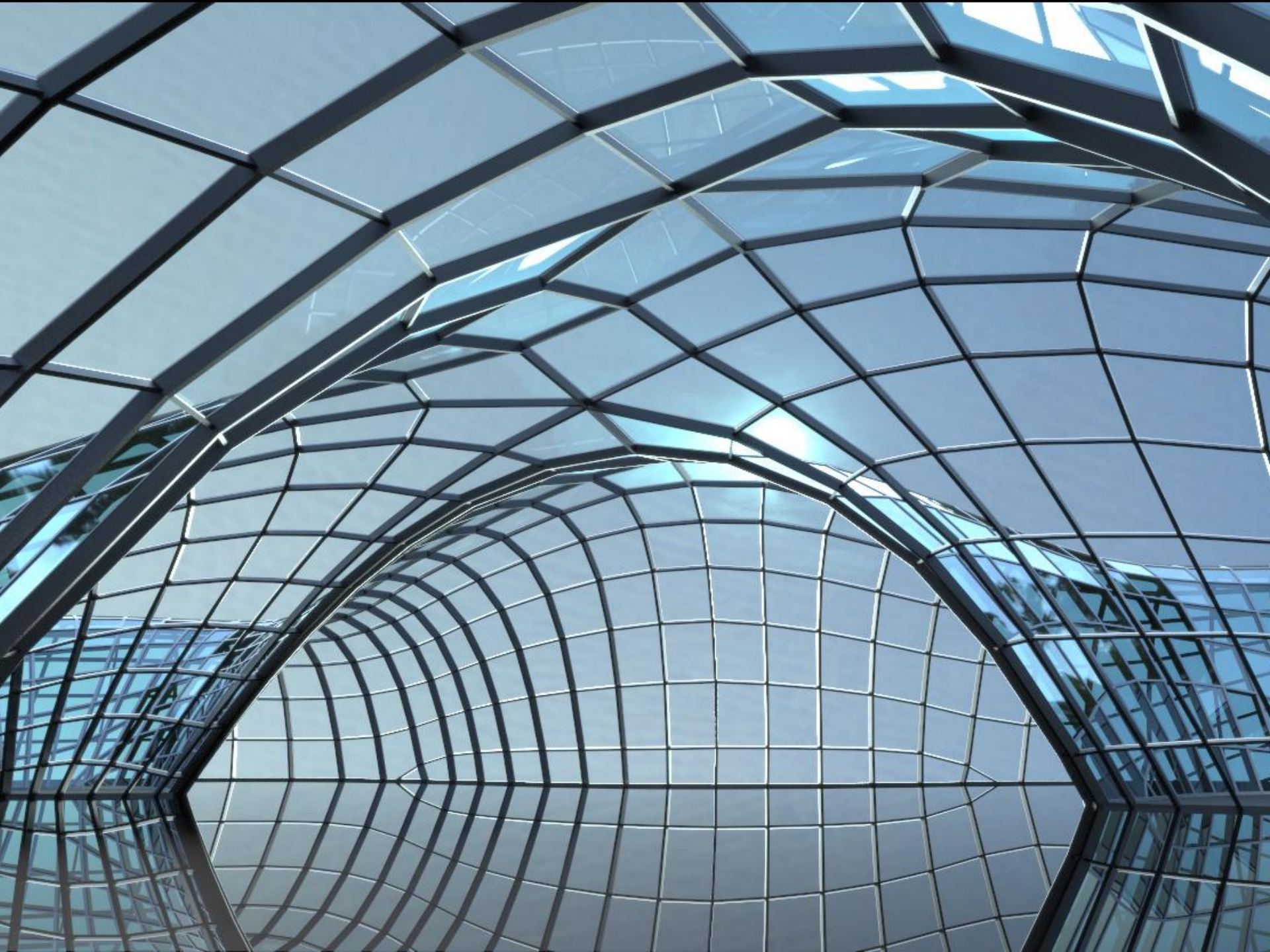
Optimization Options

- Fit network interactively
- Project vertically
- Enforce Planarity

Reset network mesh to reference mesh.

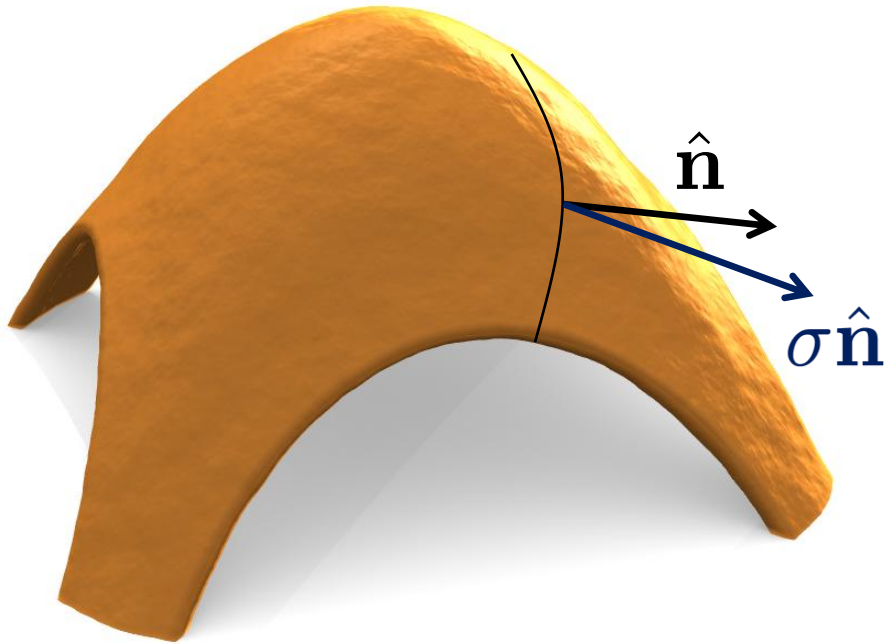






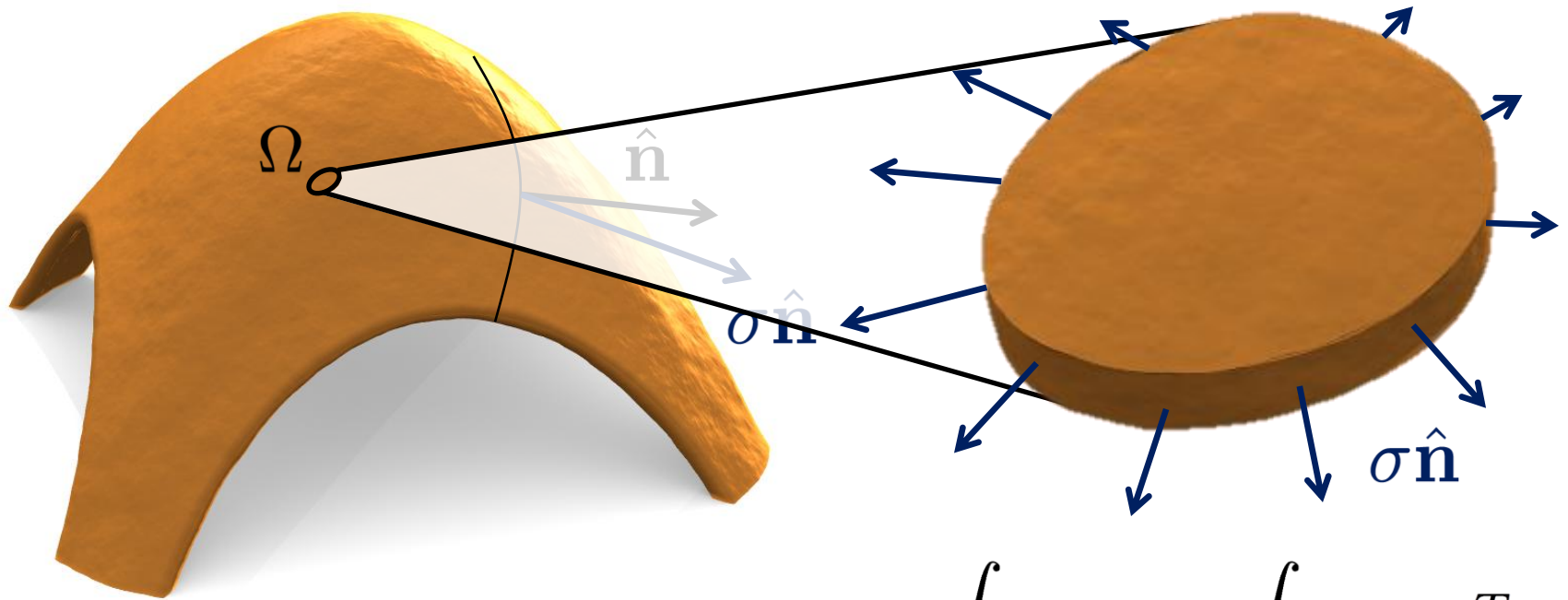
Stress Tensor

3 x 2 matrix σ measuring internal force



Membrane Equilibrium

3 x 2 matrix σ measuring internal force



$$\mathbf{F}_{\text{int}} = \int_{\partial\Omega} \sigma \hat{\mathbf{n}} = \int_{\Omega} \text{div } \sigma^T$$

Membrane Equilibrium

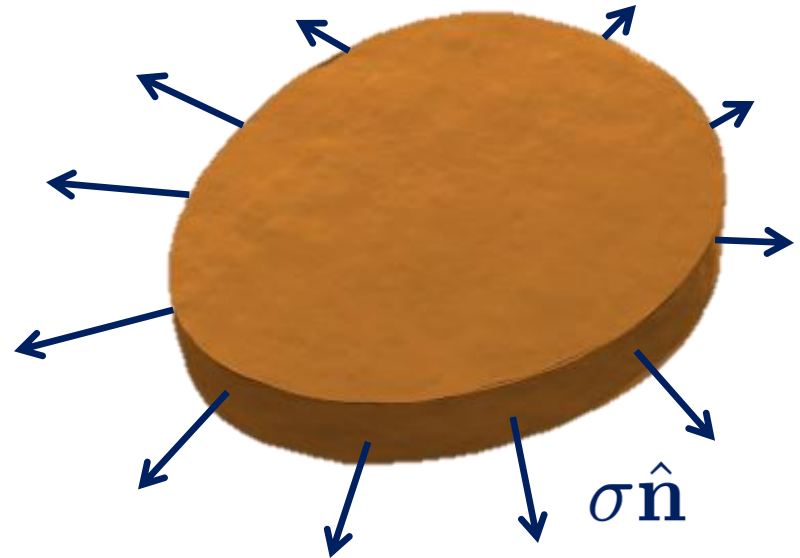
$$\operatorname{div} \sigma^T = \mathbf{F}_{\text{ext}}$$

$$\operatorname{div} (M [I \quad \nabla z]) = \mathbf{F}_{\text{ext}}$$

$$\operatorname{div} M \nabla z = F_z$$

$$\operatorname{div} M = 0$$

M positive semidefinite



$$\mathbf{F}_{\text{int}} = \int_{\partial\Omega} \sigma \hat{\mathbf{n}} = \int_{\Omega} \operatorname{div} \sigma^T$$

Stress Laplacian

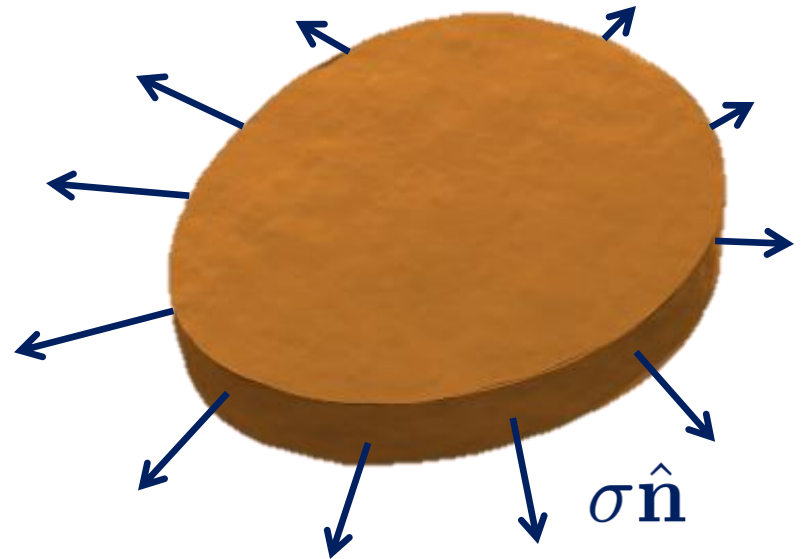
$$\operatorname{div} \sigma^T = \mathbf{F}_{\text{ext}}$$

$$\operatorname{div} (M [I \quad \nabla z]) = \mathbf{F}_{\text{ext}}$$

$$\Delta_M z \quad \cancel{\operatorname{div} M \nabla z} = F_z$$

$$\operatorname{div} M = 0$$

M positive semidefinite

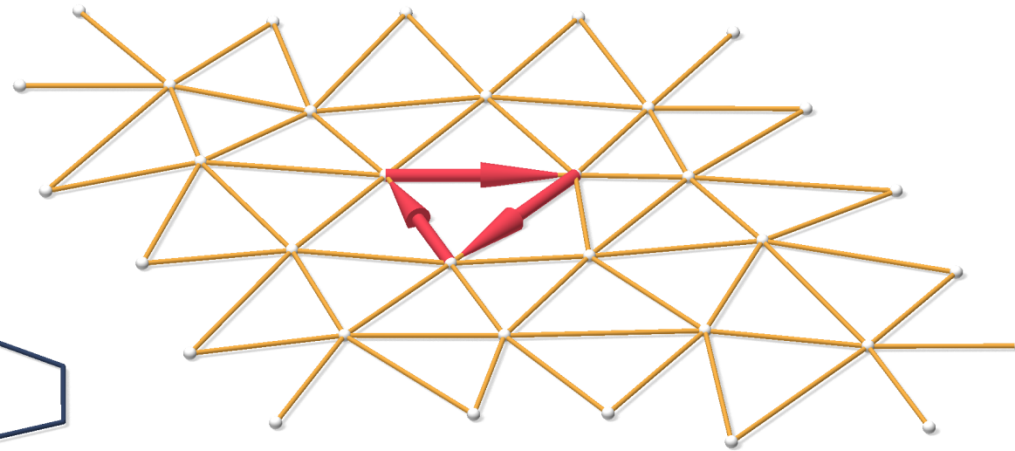
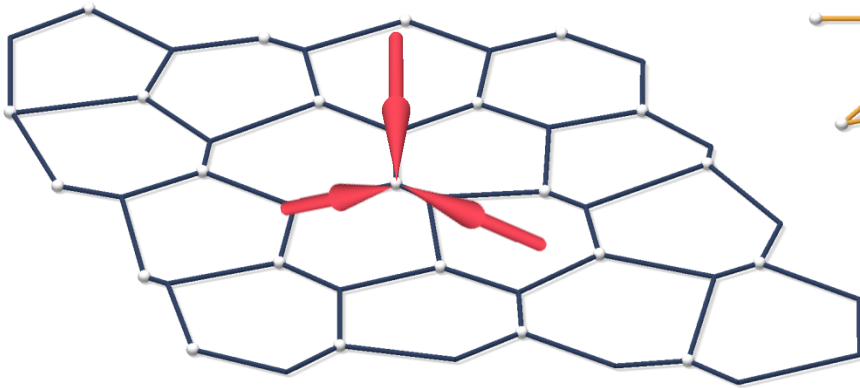


$$\mathbf{F}_{\text{int}} = \int_{\partial\Omega} \sigma \hat{\mathbf{n}} = - \int_{\Omega} \operatorname{div} \sigma^T$$

Discretization Dictionary

$z(x, y)$	z_i
$\operatorname{div} M = 0$	$\sum w_{ij}(\mathbf{v}'_i - \mathbf{v}'_j) = 0$
$\Delta_M z = \operatorname{div} M \nabla z$	$L_{\mathbf{w}} z = \sum w_{ij}(z_i - z_j)$
M positive semidefinite	$w_{ij} \geq 0$

Reciprocal Diagrams [Maxwell; Ash et al 1988]



$$\sum_{j \sim i} w_{ij} (\mathbf{v}'_i - \mathbf{v}'_j) = 0$$

$$\sum_{j \sim i} w_{ij} (\mathbf{v}'_i - \mathbf{v}'_j)^\perp = 0$$

Equilibrium Equations

edge
weights

Stress
Laplacian

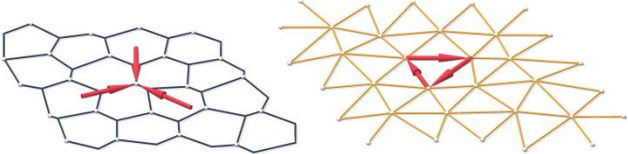


Equilibrium Equations



horizontal equilibrium

Reciprocal Diagrams



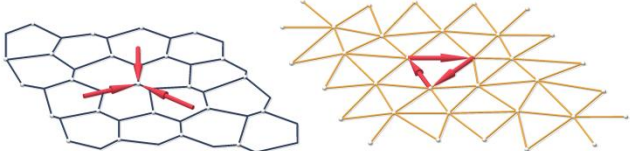
Stress Laplacian

Equilibrium Equations



horizontal equilibrium

Reciprocal Diagrams



DEC



Stress Laplacian



edge weights

Airy Stress Potential

$$M = \begin{bmatrix} \phi_{yy} & -\phi_{xy} \\ -\phi_{xy} & \phi_{xx} \end{bmatrix}$$
$$= (\nabla^2 \phi)^{-1} \det \nabla^2 \phi$$

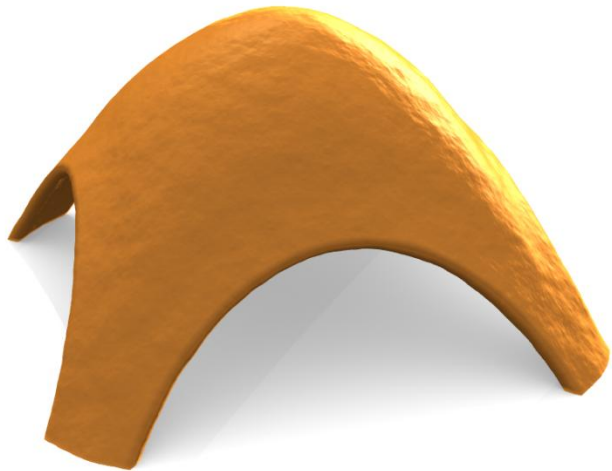
recall:

$$\operatorname{div} M \nabla z = F_z$$

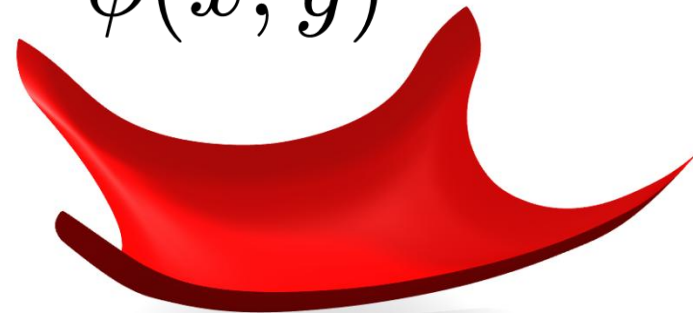
$$\operatorname{div} M = 0$$

$$M \geq 0$$

$z(x, y)$

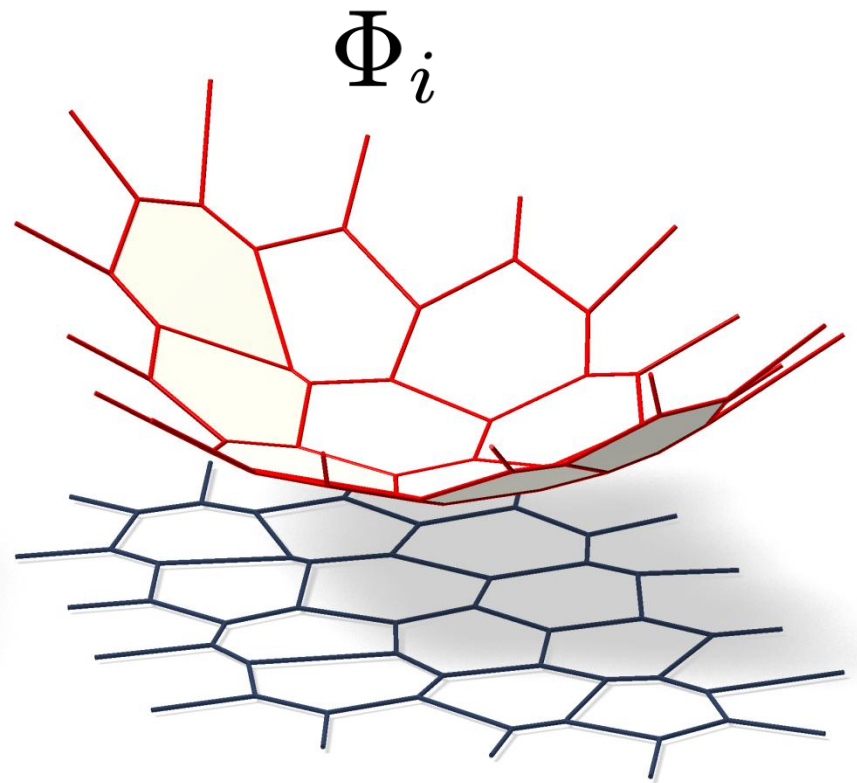
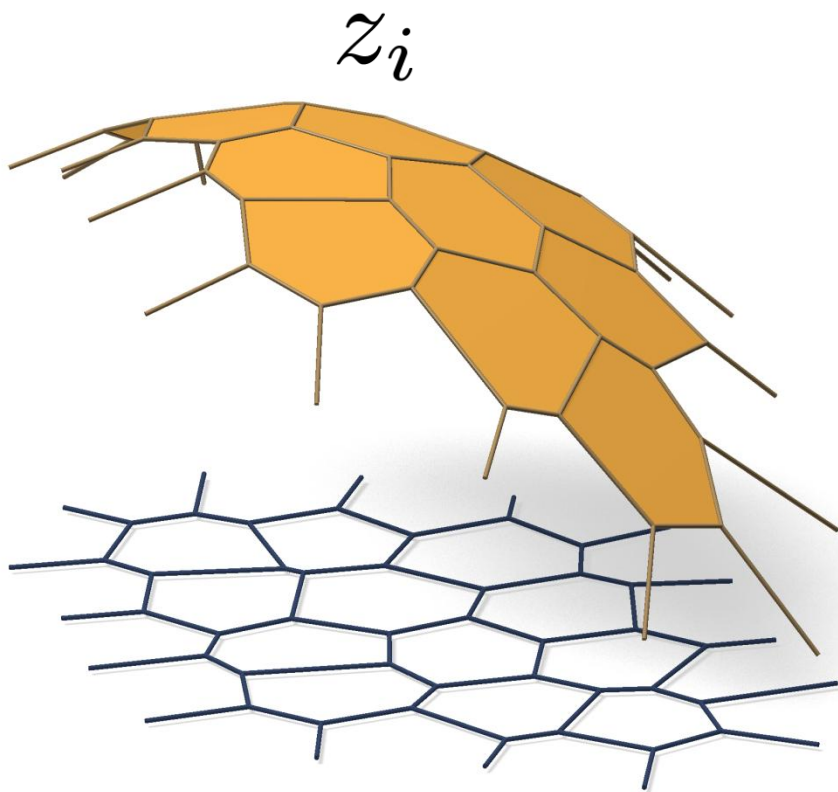


$\phi(x, y)$



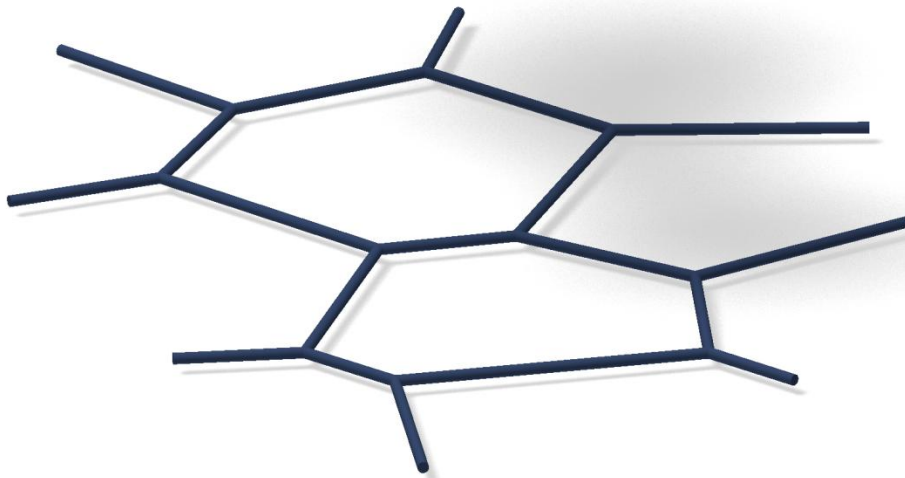
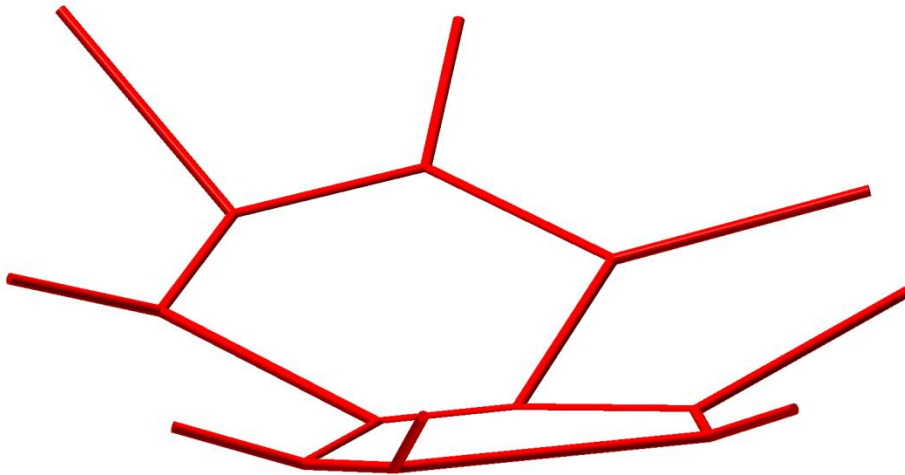
convex

Airy Stress Polytope [Fraternali 2010]

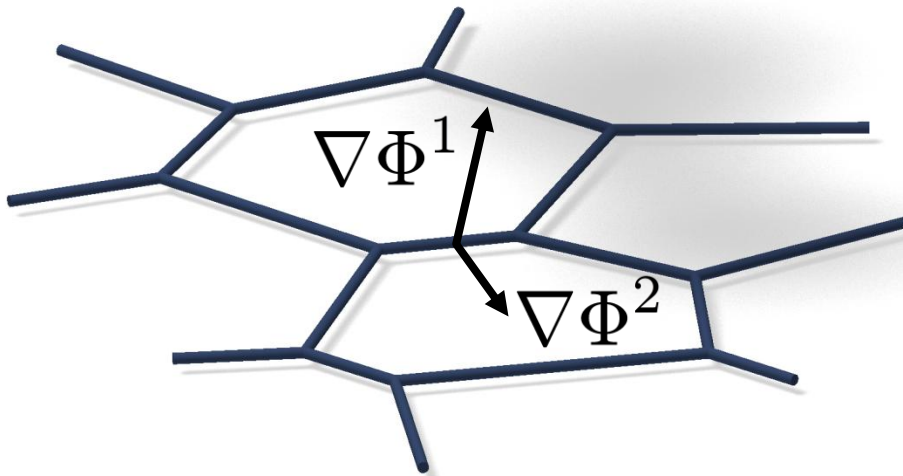
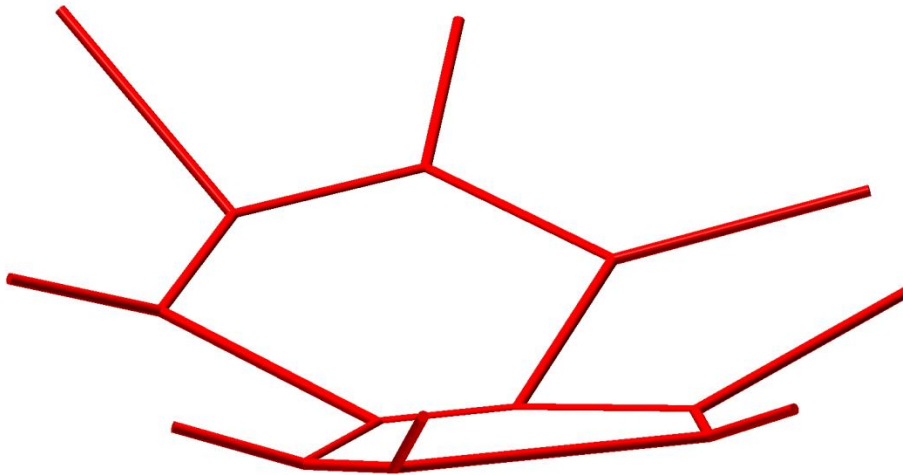


convex, planar faces

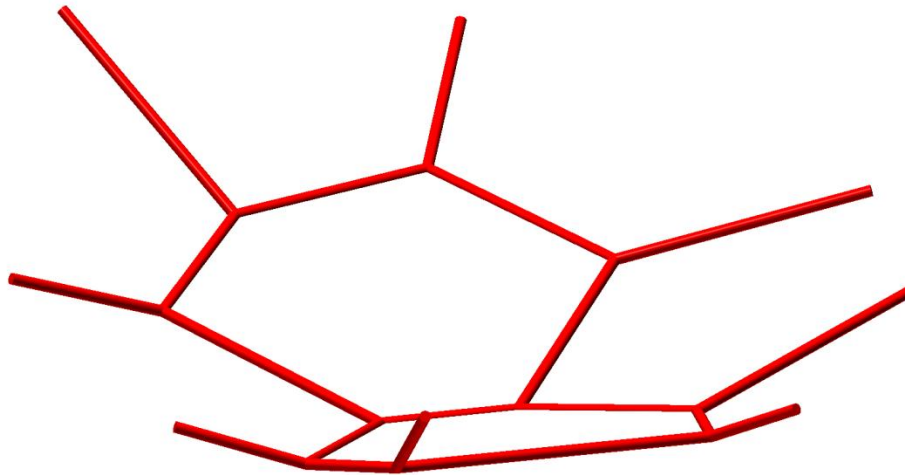
Stress Polytope: Gradient Jumps



Stress Polytope: Gradient Jumps

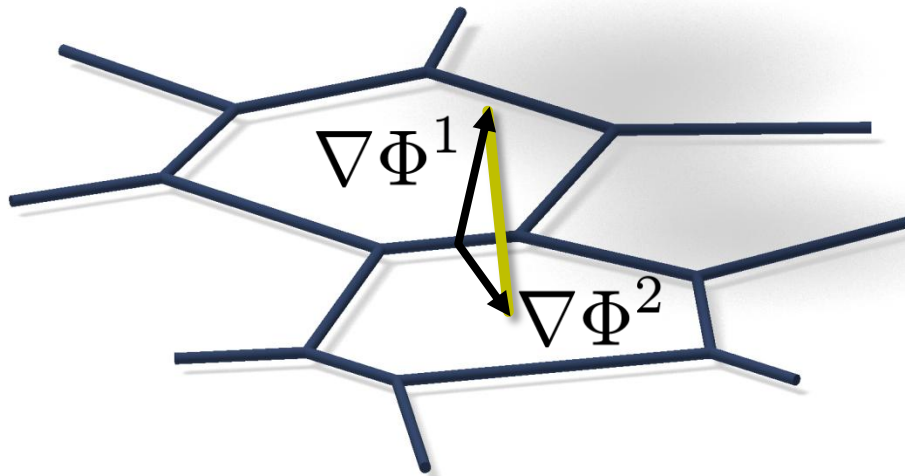


Stress Polytope: Gradient Jumps

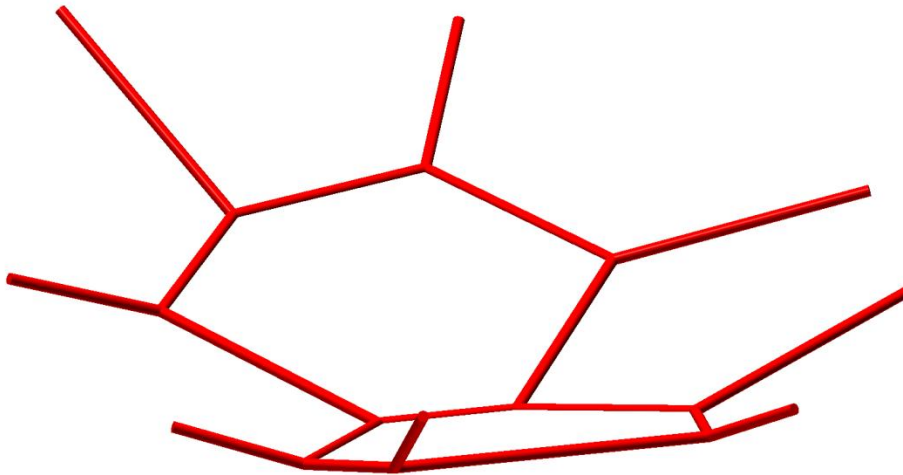


dual edge

$$\tilde{\mathbf{e}}_{ij} = \nabla \Phi^j - \nabla \Phi^i$$

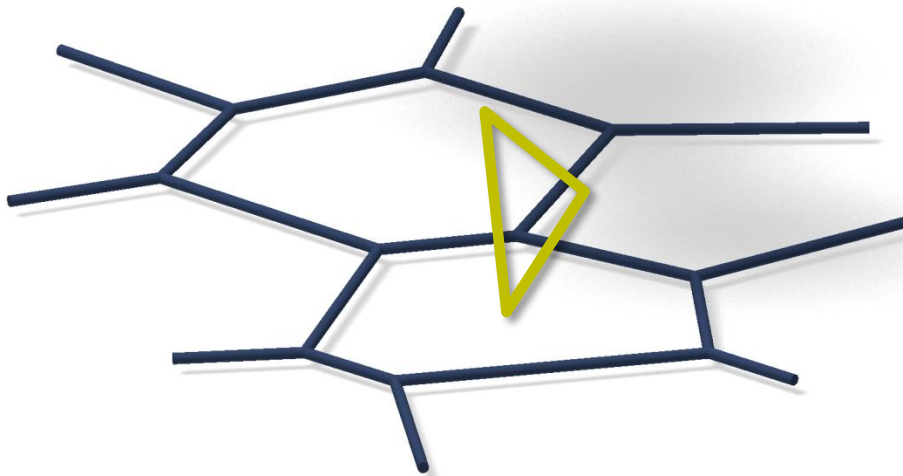


Stress Polytope: Gradient Jumps

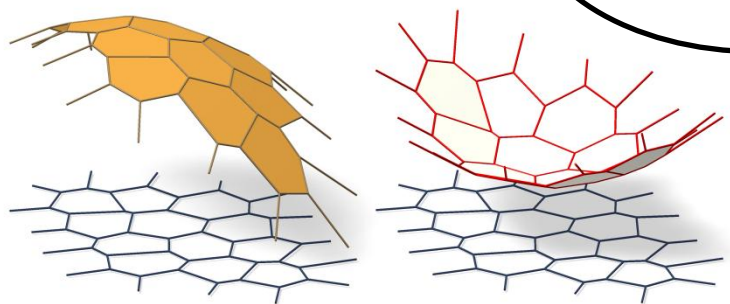
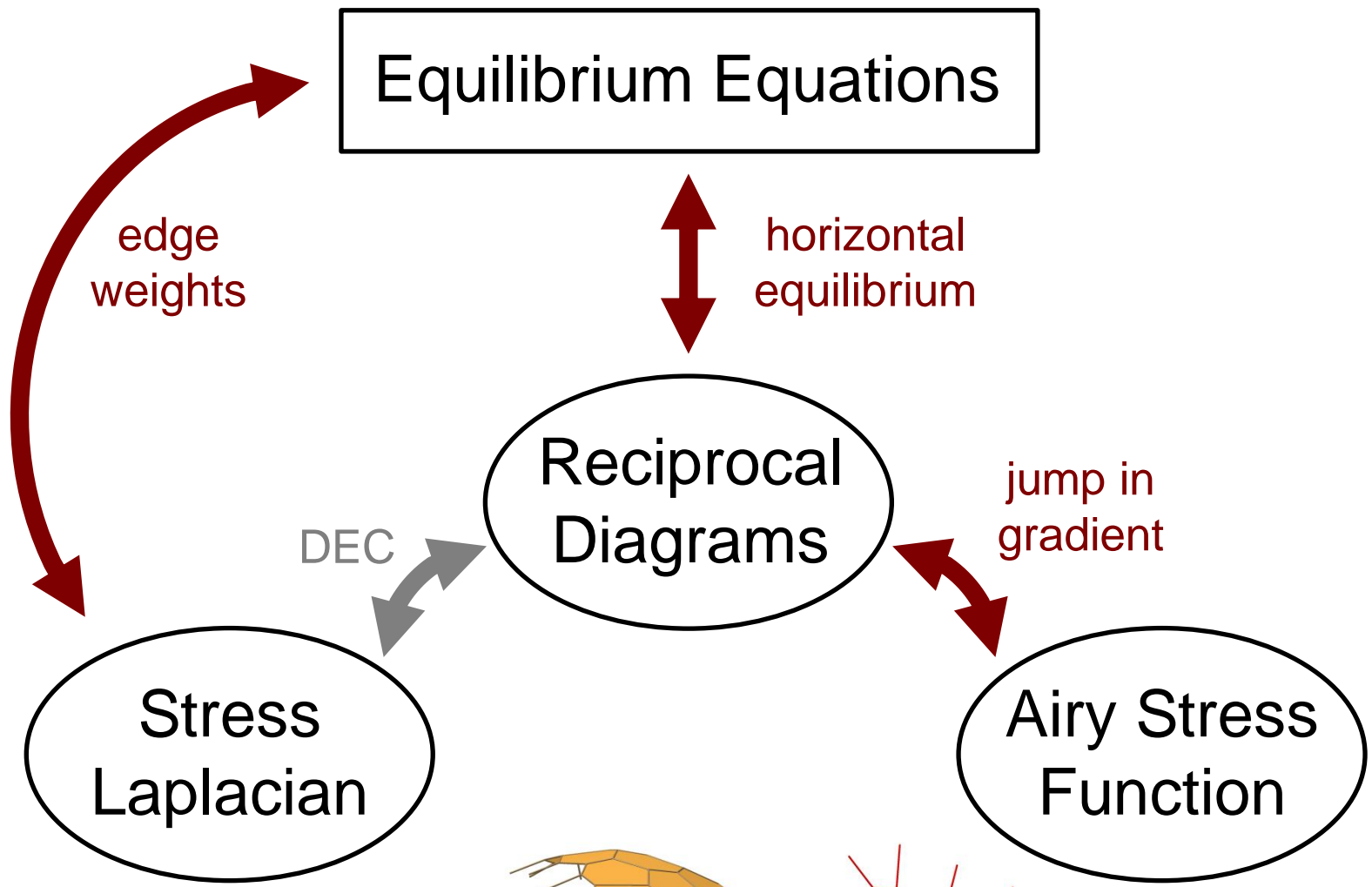


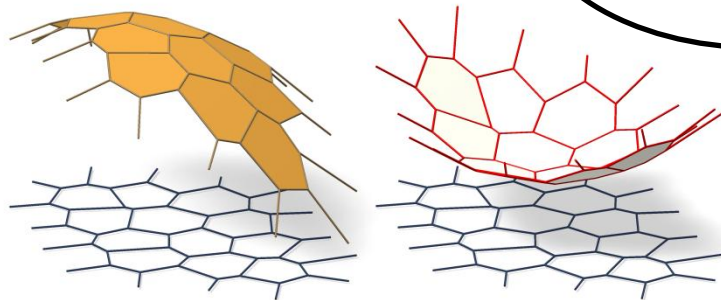
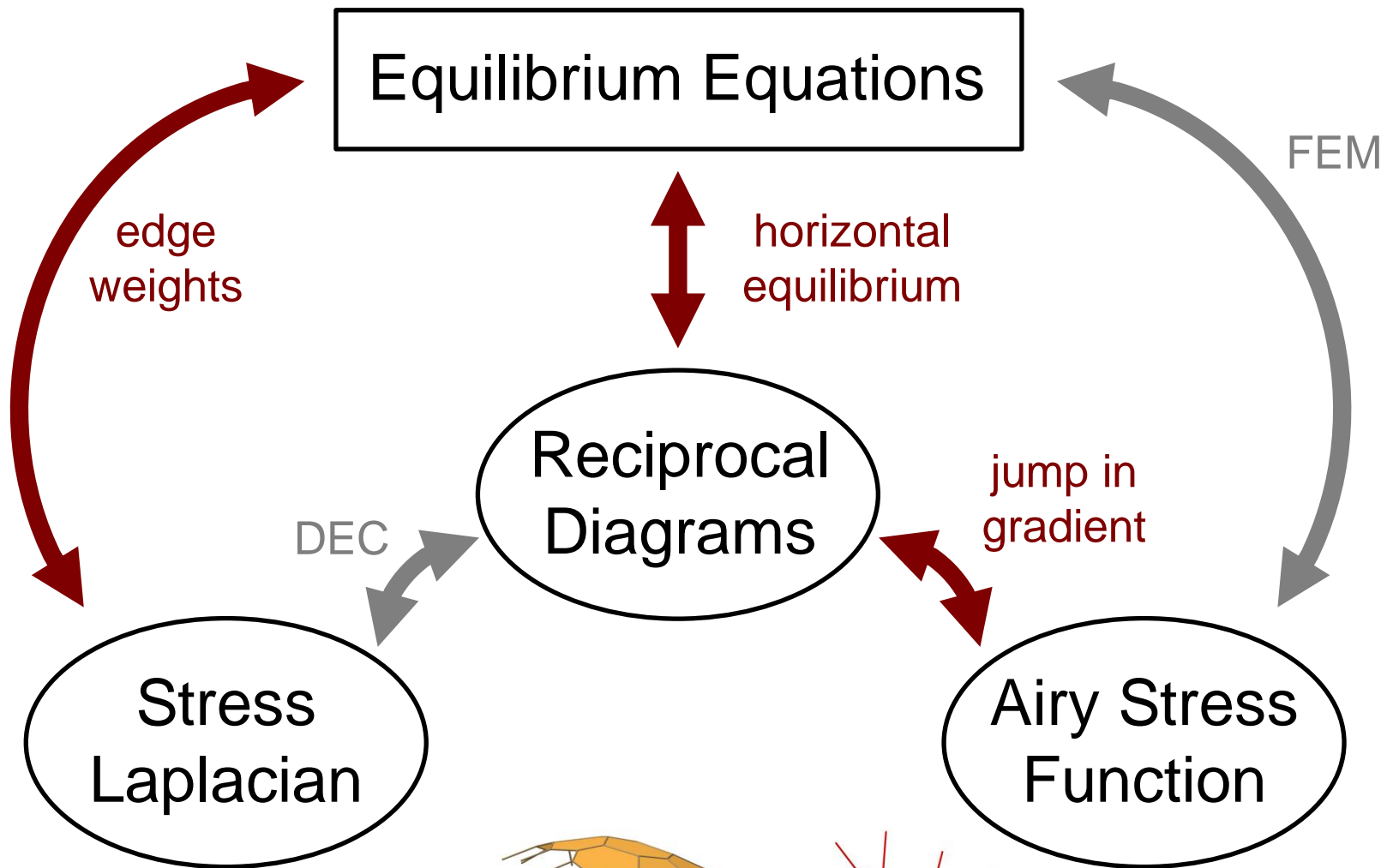
dual edge

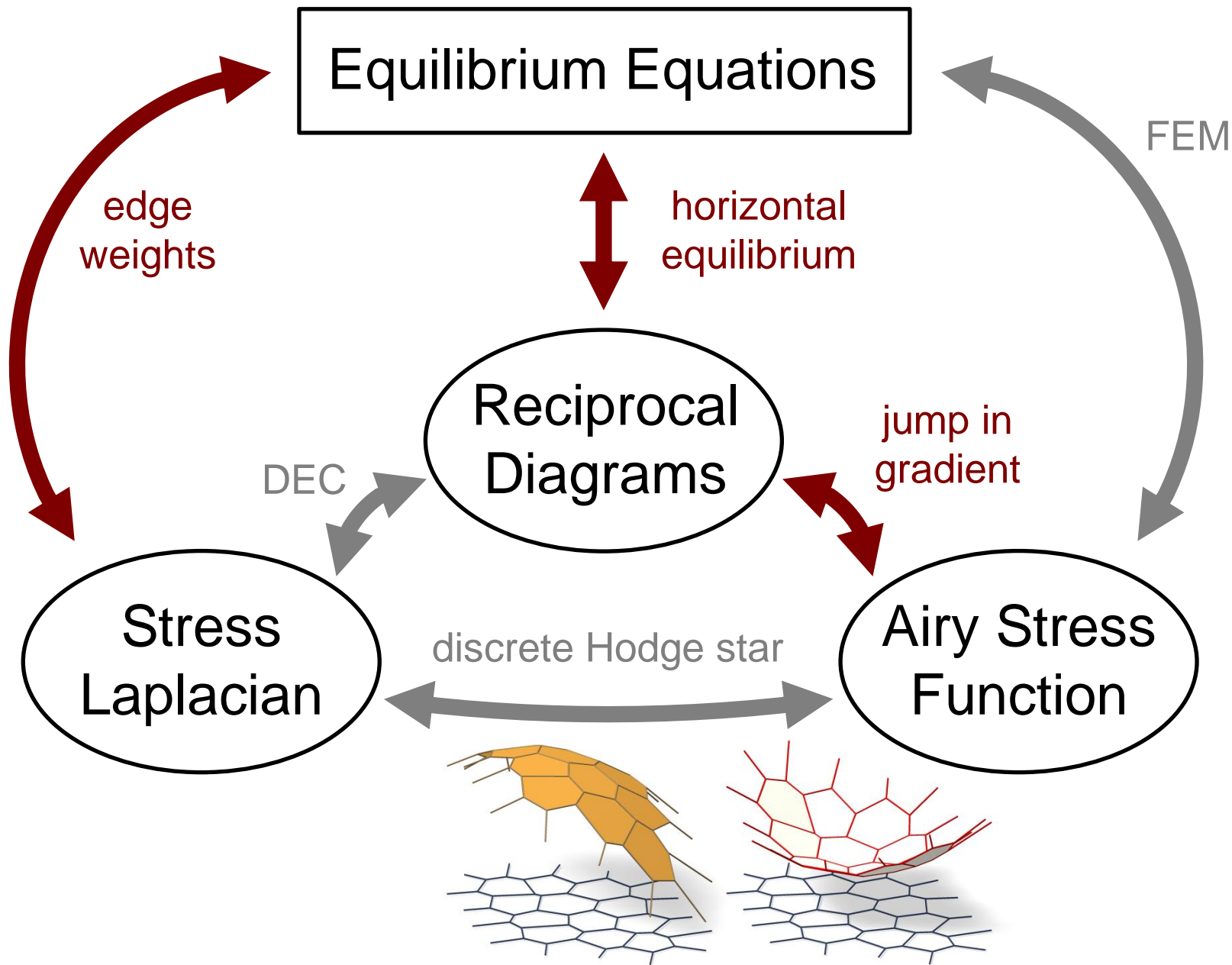
$$\tilde{\mathbf{e}}_{ij} = \nabla \Phi^j - \nabla \Phi^i$$



$$\tilde{\mathbf{e}}'_{12} + \tilde{\mathbf{e}}'_{23} + \tilde{\mathbf{e}}'_{31} = 0$$







Relative Curvatures

recall:

$$\operatorname{div} M \nabla z = F_z$$

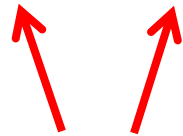
$$\operatorname{div} M = 0$$

$$M \geq 0$$

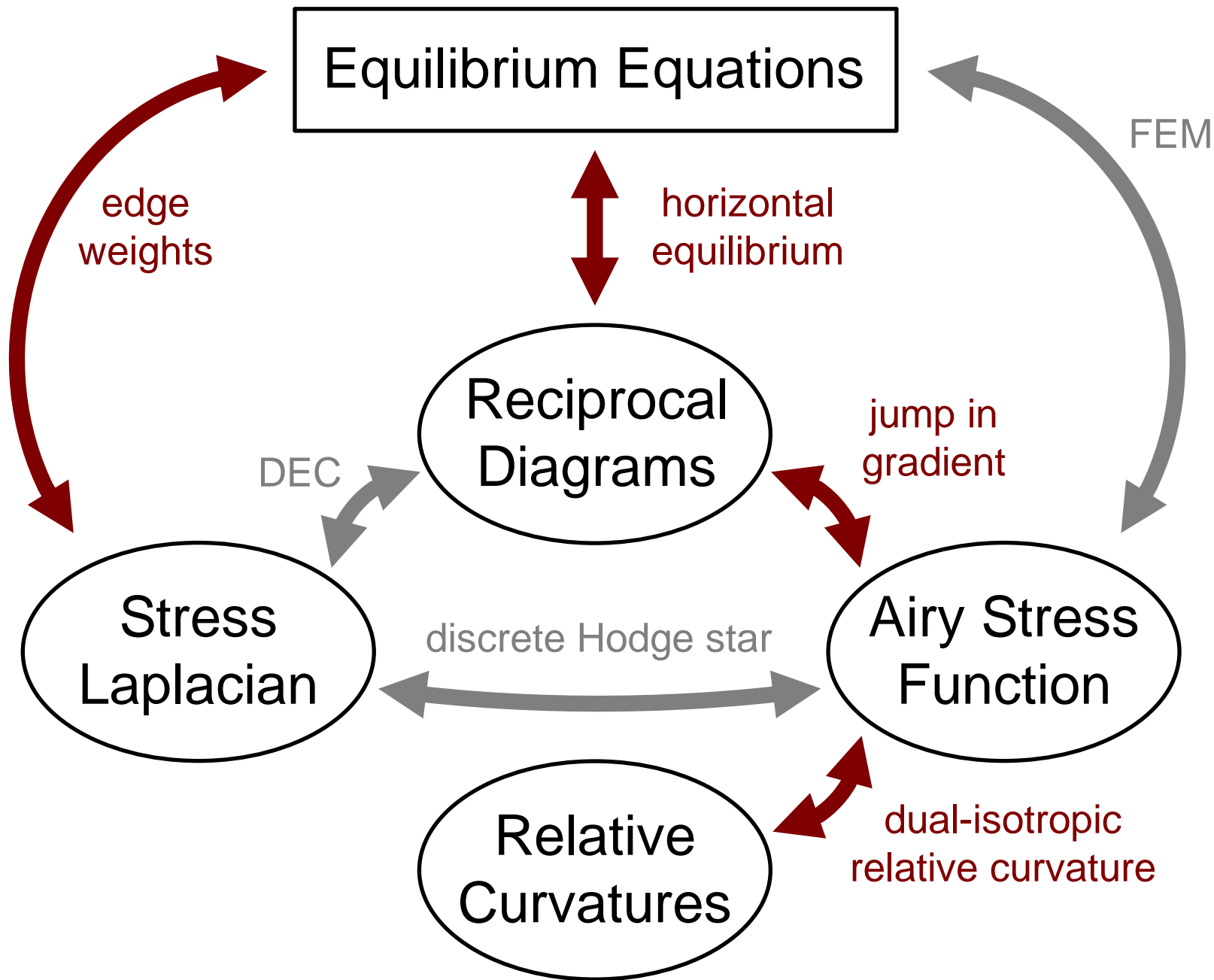
$$\operatorname{div} M \nabla z = \operatorname{tr} \left[(\nabla^2 \phi)^{-1} (\nabla^2 z) \right] \det \nabla^2 \phi$$

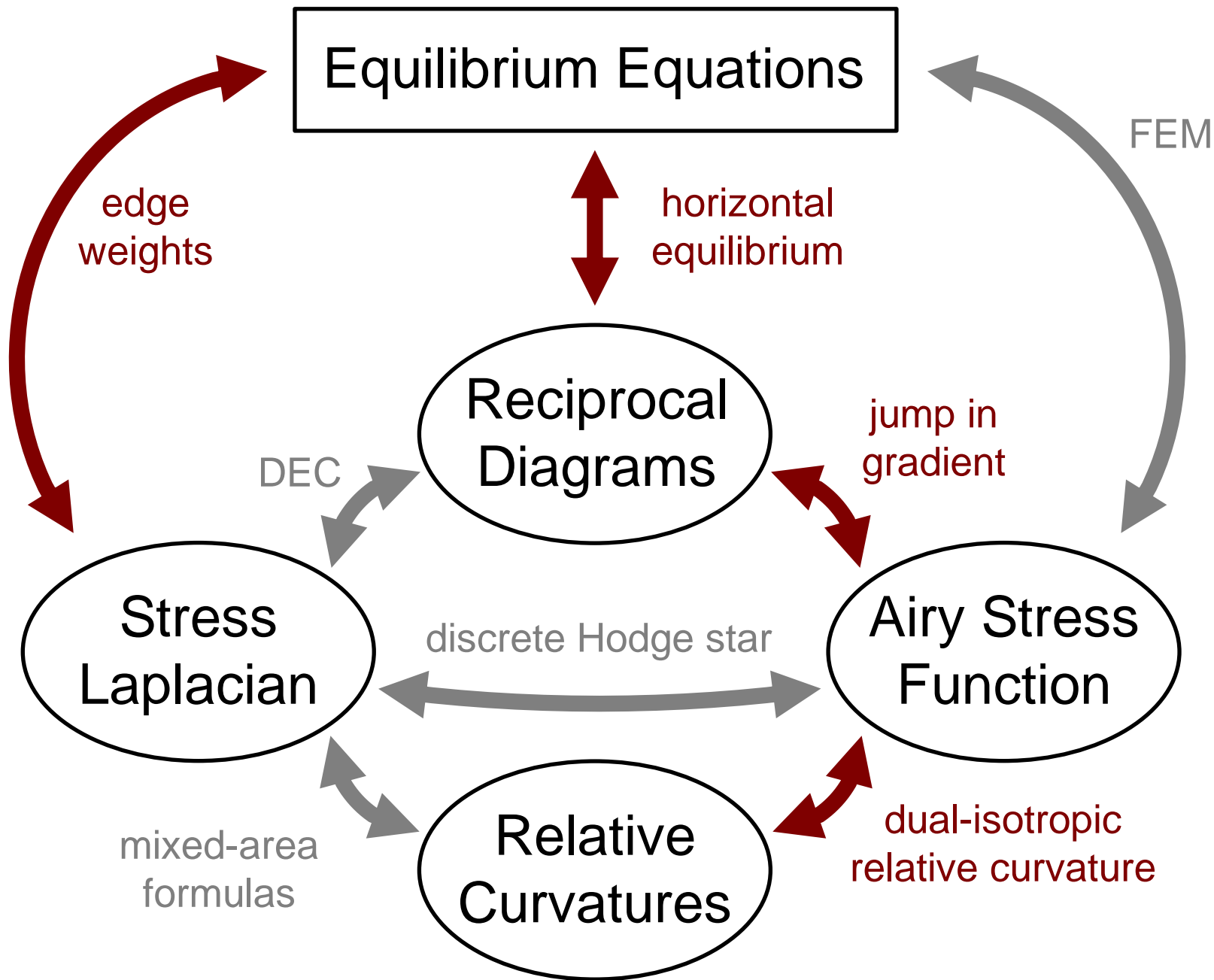
looks like curvatures!

$$2H^{z, \phi} K^{\phi, (x^2 + y^2)/2} = F_z$$

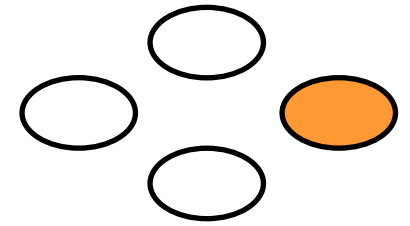


“dual-isotropic relative mean and Gaussian curvatures”

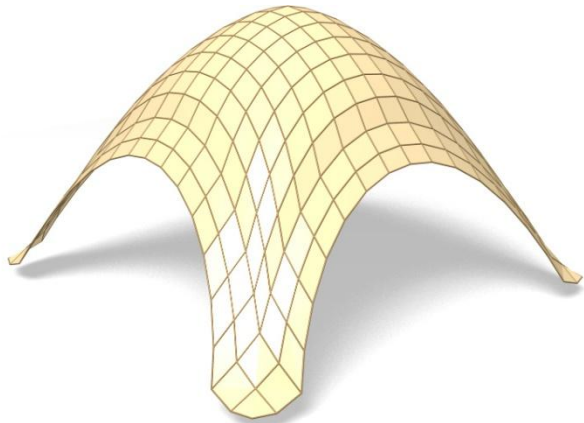




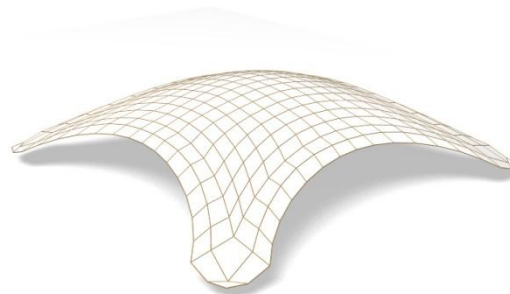
PQ Remeshing



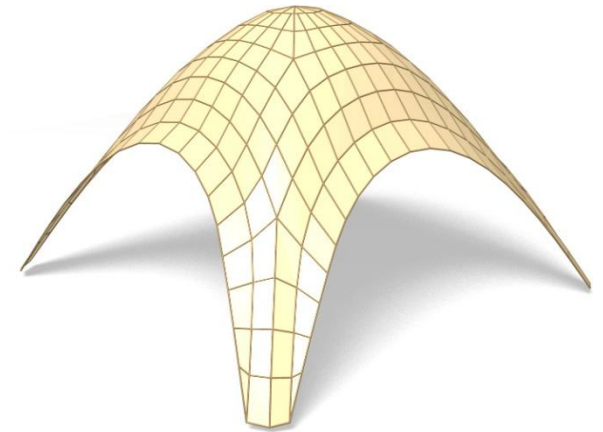
Airy Stress Function



Original



Naïve
Optimization

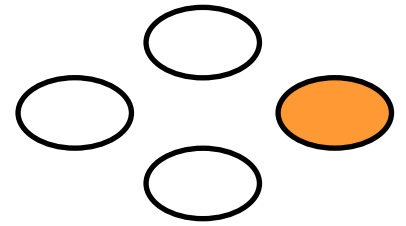
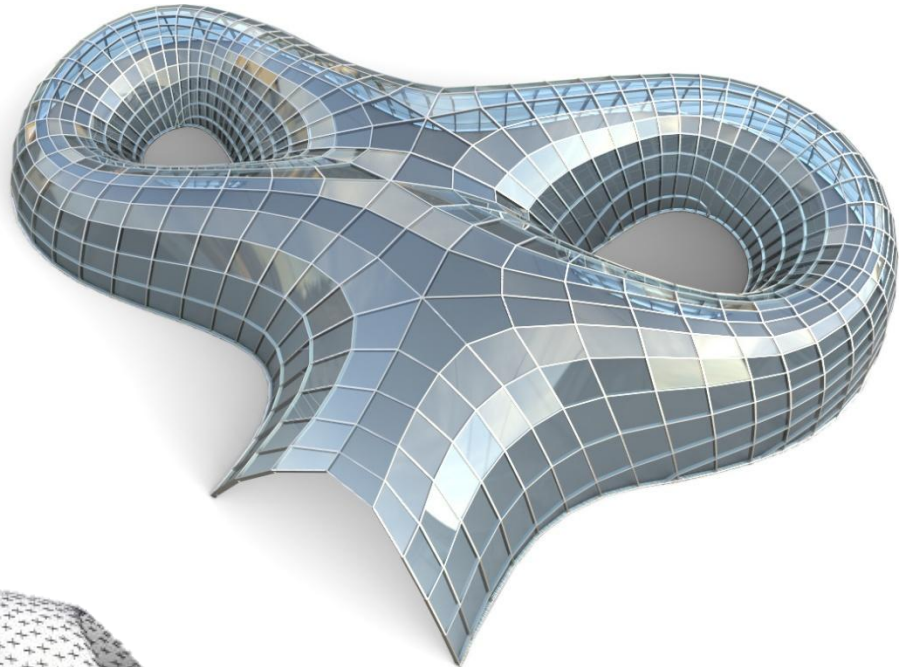
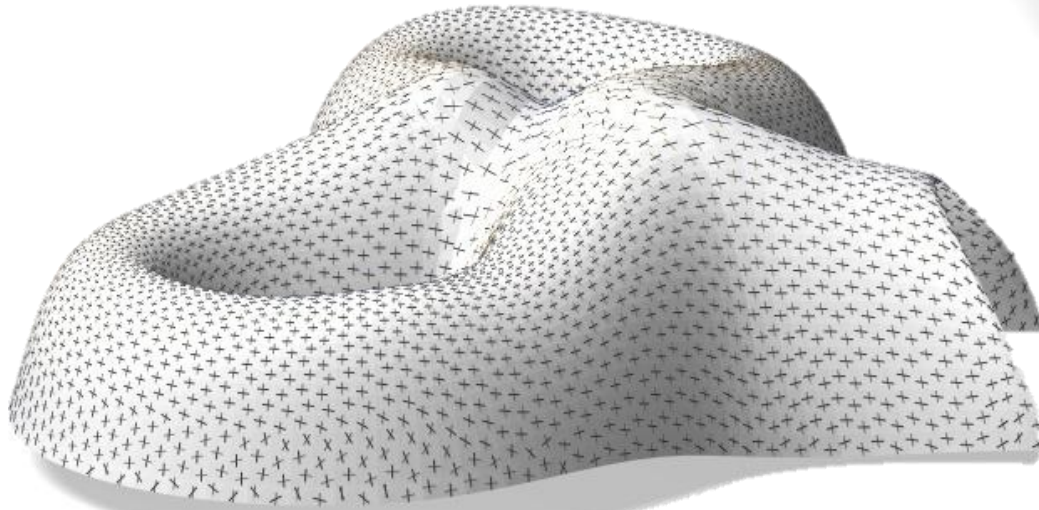


Using Airy
Polytope

PQ Remeshing

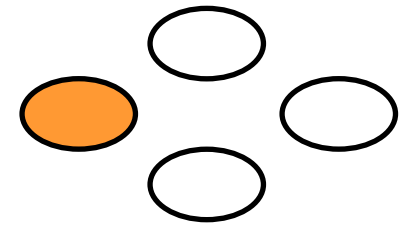
Remesh along
eigenvectors of

$$(\nabla^2 \phi)^{-1} (\nabla^2 z)$$



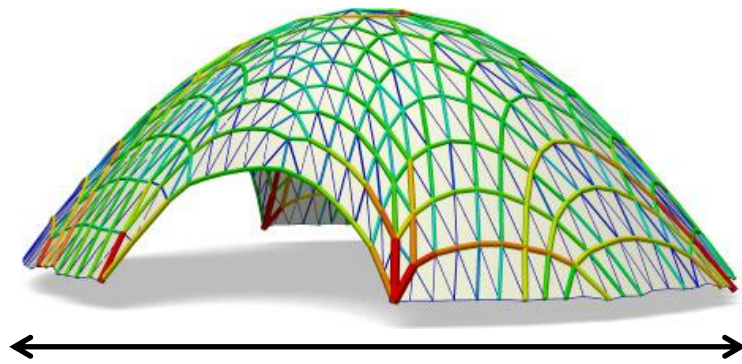
Airy Stress Function

Loading of Surface

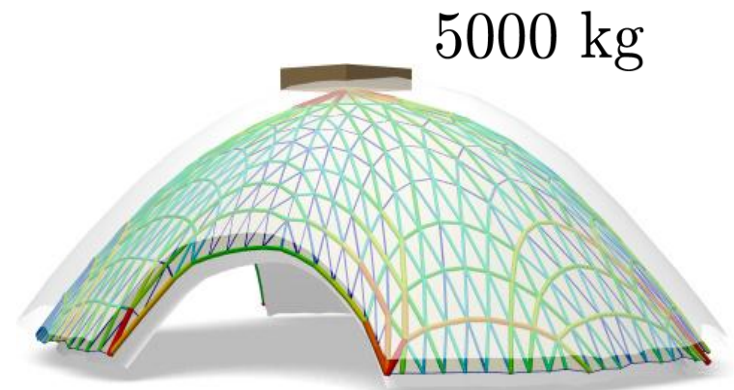


Stress Laplacian

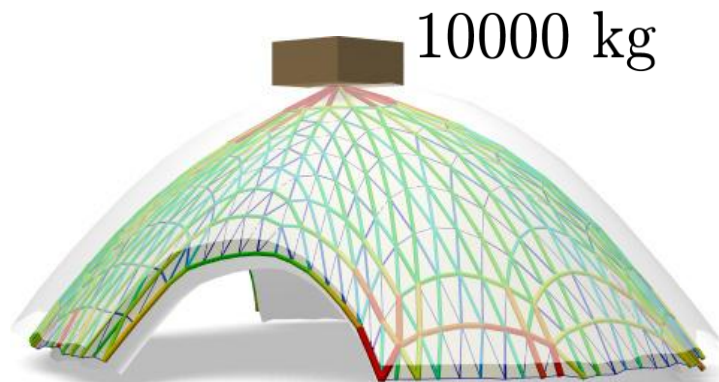
Shell thickness 0.1 m, $\rho = 2500 \text{ kg/m}^3$



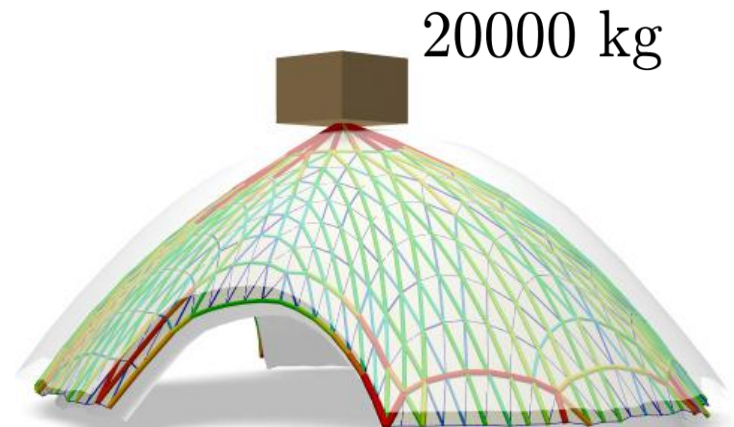
14 m



5000 kg

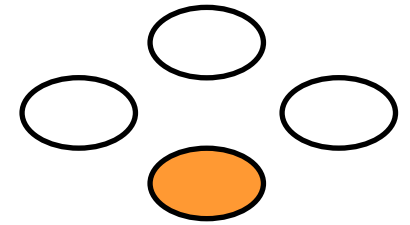


10000 kg



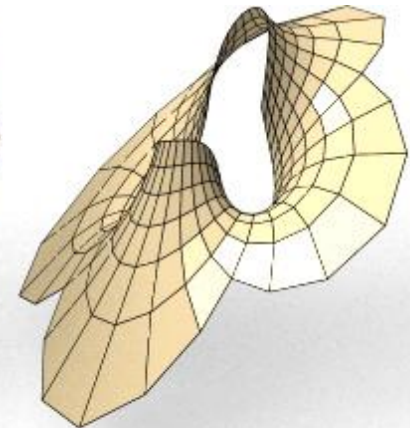
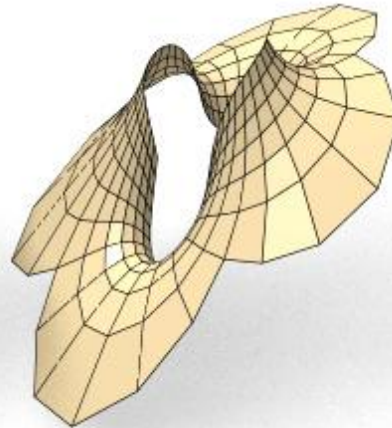
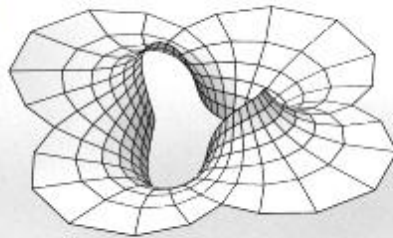
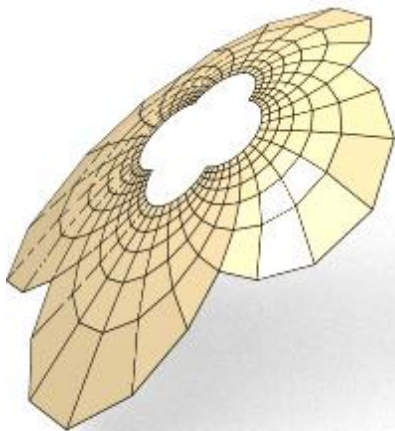
20000 kg

Special Families



Relative Curvatures

$$\text{Recall: } 2H^{z,\phi} K^{\phi,(x^2+y^2)/2} = F_z$$

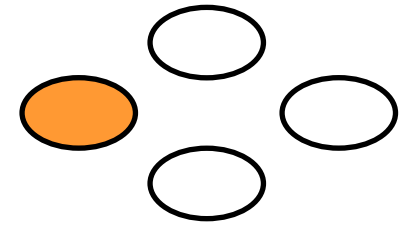


Template

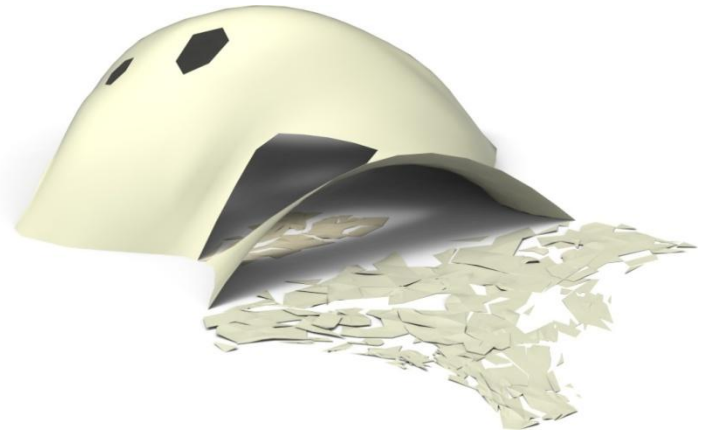
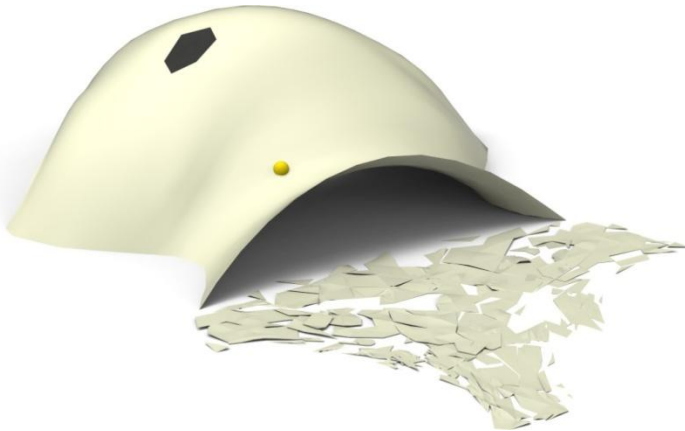
$$H^{z,\phi} = 0$$

Linear Combinations

Surface Destruction



Stress Laplacian



What's Next?

Non-vertical loads

wind, earthquakes, ...

Non-manifold surfaces

T junctions, flying buttresses, ...

Can we further exploit geometrization
of equilibrium?

Thank You!

Miklós Bergou

Adobe

Philippe Block

ATI

Eitan Grinspun

Autodesk

Florin Isvoranu

mental images

Danny Kaufman

NVIDIA

Niloy Mitra

Side Effects Software

Alexander Schiffner

Walt Disney Company

Weta Digital

